

**MODELLING BIOLOGICAL MACROMOLECULES IN SOLUTION:  
THE GENERAL TRI-AXIAL ELLIPSOID**

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Appendix V FORTRAN IV computer programs

- Program 1: Evaluates values of the various hydrodynamic shape functions for tri-axial ellipsoids for a user specifiable value of the axial ratios ( $a/b$ ,  $b/c$ )
- Program 2: Produces tables of these functions for axial ratios between 1.0 and 2.0 in steps of 0.1
- Program 3: Produces a contour map of  $v$  in the  $(a/b, b/c)$  plane for axial ratios between 1.0 and 3.0
- Program 4: Produces plots of the various tri-axial functions in the  $(a/b, b/c)$  plane corresponding to the point (1.5, 1.5). Several plots allow for arbitrary errors in measurement
- Program 5: Non-linear least squares iterative method for resolving a 2-term exponential birefringence decay. This program (and the following two) produces its own synthetic data
- Program 6: Fourier Transform solution of the Laplace Integral Equation method
- Program 7: R-constrained non-linear least squares iterative method

<u>Function</u>	<u>Computer Symbol</u>
a/b	A/B
b/c	B/C
v	NU, S
f/f <sub>o</sub> ( $\equiv P$ )	F
$\zeta_a/\zeta_o$	CA, CA/CO
$\zeta_b/\zeta_o$	CB, CB/CO
$\zeta_c/\zeta_o$	CC, CC/CO
$\rho_a/\rho_o$	RHOA, RHOA/RHOO
$\rho_b/\rho_o$	RHOB, RHOB/RHOO
$\rho_c/\rho_o$	RHOC, RHOC/RHOO
$\beta$	BETA
R	R
$\delta_a$	DELTA(A)
$\delta_b$	DELTA(B)
$\delta_c$	DELTA(C)
$\gamma_a$	GAMMA(A)
$\gamma_b$	GAMMA(B)
$\gamma_c$	GAMMA(C)
$\mu_a$	MU(A)
$\mu_b$	MU(B)
$\mu_c$	MU(C)
$\tau_h/\tau_o$	TAU, TAU/TAUO
$\Psi$	PSI
$\Lambda$	LAMBDA
$\theta_+^{red}$	TPLS, THETA+, Z
$\theta_-^{red}$	TMNS, THETA-, U

<u>Function</u>	<u>Computer Symbol</u>
$\delta_+$	DPLS, DELTA+, V
$\delta_-$	DMNS, DELTA-, W
$\gamma_+$	GPLS, GAMMA+
$\gamma_-$	GMNS, GAMMA-
$\tau_1/\tau_o$	T1
$\tau_2/\tau_o$	T2
$\tau_3/\tau_o$	T3
$\tau_4/\tau_o$	T4
$\tau_5/\tau_o$	T5
$\theta_+$	THPLUS
$\theta_-$	THMNUS

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***** THIS PROGRAM GENERATES VALUES OF THE VARIOUS HYDRODYNAMIC
      SHAPE FUNCTIONS FOR A USER SPECIFIABLE VALUE OF THE AXIAL
      RATIOS A/B (=N1) & B/C (=N2)
***** PROGRAM MAIN(INPUT,OUTPUT,TAPE2=INPUT,TAPE3=OUTPUT)
COMMON/PARAM/A,C,NN
EXTERNAL FUN
DIMENSION ALPHA(10)
REAL NU,M,O,P
REAL MUA,MUB,MUC,PSI,N1,N2,RHOA,RHOB,RHOC
C ENTER AS DATA AT THE FOOT OF THE PROGRAM (A/B, B/C)
READ(2,*) N1,N2
NN=0
C COMPUTE THE ELLIPTIC INTEGRALS
D045 K=1,10
A=N1
B=1.0
C=1.0/N2
NN=NN+1
C SET LIMITS FOR NUMERICAL INTEGRATION (THESE LIMITS
BELOW HAVE BEEN PREVIOUSLY TESTED FOR CONVERGENCE)
AA=0.0
BB=10000000
IF(NN.EQ.10)BB=500000000
MAXDIV=50
EPS=1.0E-08
ACC=0.0
IFAIL=0
C CALL U.K. "NAG" LIBRARY ROUTINE FOR NUMERICAL EVALUATION
OF THE INTEGRALS "ALPHA" GIVEN IN THE SUBROUTINE BELOW
CALL D01AGF(AA,BB,FUN,MAXDIV,EPS,ACC,ANS,ERROR,NOFUN,IFAIL)
ALPHA(NN)=ANS
45 CONTINUE
B=1.0
C NOW COMPUTE THE FUNCTION VALUES USING THE STORED INTEGRAL VALUES
NU=(1.0/(A*B*C))*((4.0/15.0)*((ALPHA(7)+ALPHA(8)
+ +ALPHA(9))/(ALPHA(8)*ALPHA(9)+ALPHA(9)*ALPHA
+ (7)+ALPHA(7)*ALPHA(8)))+(1.0/5.0)*((ALPHA(2)
+ +ALPHA(3))/(ALPHA(4)*(B*B*ALPHA(2)+C*C*ALPHA(3)
+ ))+((ALPHA(3)+ALPHA(1))/(ALPHA(5)*(C*C*ALPHA(3)
+ +A*A*ALPHA(1))))+((ALPHA(1)+ALPHA(2))/(ALPHA(6)
+ +(A*A*ALPHA(1)+B*B*ALPHA(2))))))
M=(B*B+C*C)/(B*B*ALPHA(2)+C*C*ALPHA(3))
O=(C*C+A*A)/(C*C*ALPHA(3)+A*A*ALPHA(1))
P=(A*A+B*B)/(A*A*ALPHA(1)+B*B*ALPHA(2))
TPLS=((A*B*C)/(12.0))*(((1.0/M)+(1.0/O)+(1.0/P
+ ))+((1.0/M**2.0)+(1.0/O**2.0)+(1.0/P**2.0))-_
+ ((1.0/(M*O))+(1.0/(O*P))+(1.0/(P*M
+ )))*0.5))
TMNS=((A*B*C)/(12.0))*(((1.0/M)+(1.0/O)+(1.0/P
+ ))-((1.0/M**2.0)+(1.0/O**2.0)+(1.0/P**2.0))-_
+ ((1.0/(M*O))+(1.0/(O*P))+(1.0/(P*M
+ )))*0.5))
DPLS=6.0*TPLS*NU
DMNS=6.0*TMNS*NU
F=2.0/(((A*B*C)**(1.0/3.0))*ALPHA(10))
R=2.0*(1.0+(F**3.0))/NU
BETA=(1.0/1000000.0)*(((6.0249**(1.0/3.0))*(10.0**23.0/3.0
+ ))/((16200.0*3.141592654*3.141592654)**(1.0/3.0)))*(NU
+ *(1.0/3.0))/F
CA=(2.0/(3.0*A*B*C))*M
CB=(2.0/(3.0*A*B*C))*O
CC=(2.0/(3.0*A*B*C))*P
RHOA=2.0/((1.0/CB)+(1.0/CC))
RHOB=2.0/((1.0/CC)+(1.0/CA))
RHOC=2.0/((1.0/CA)+(1.0/CB))
DELA=NU/CA
DELB=NU/CB
DELCA=NU/CC
TAU=3.0/((1.0/CA)+(1.0/CB)+(1.0/CC))
PSI=F*((1.0/TAU)**(1.0/3.0))
V=NU/TAU
ZZ=(1.0/2.0)*(F**3.0)
GAMMAA=ZZ*((1.0/CB)+(1.0/CC))
GAMMAB=ZZ*((1.0/CC)+(1.0/CA))
GAMMAC=ZZ*((1.0/CA)+(1.0/CB))
MUA=(CA**2.0)/F
MUB=(CB**2.0)/F
MUC=(CC**2.0)/F
GPLS=6.0*TPLS*(F**3.0)

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GMNS=6.0*TMNS*(F**3.0)
X1=0.5*((1.0/RHOB)+(1.0/RHOC)-(1.0/RHOA))
X2=0.5*((1.0/RHOC)+(1.0/RHOA)-(1.0/RHOB))
X3=0.5*((1.0/RHOA)+(1.0/RHOB)-(1.0/RHOC))
X4=(X1+X2+X3)/3.0
X5=((X1**2.0)+(X2**2.0)+(X3**2.0)-(X1*X2)-(X2*X3)-(X3*X1))
+*#0.5
T1=1.0/(X4+X1)
T2=1.0/(X4+X2)
T3=1.0/(X4+X3)
T4=3.0/((6.0*X4)-(2.0*X5))
T5=3.0/((6.0*X4)+(2.0*X5))
WRITE(3,97)
97 FORMAT( "   ")
WRITE(3,98)
98 FORMAT( "   ")
WRITE(3,99)A,1/C
99 FORMAT(5X," A/B    F7.2,"    B/C    ",F7.2)
WRITE(3,100)NU
100 FORMAT(5X," NU  ",F10.5)
WRITE(3,106)F
106 FORMAT(5X," F  ",F10.5)
WRITE(3,101)TPLS
101 FORMAT(5X," THETA+  ",F15.5)
WRITE(3,102)TMNS
102 FORMAT(5X," THETA-  ",F15.5)
WRITE(3,103)DPLS
103 FORMAT(5X," DELTA+  ",F15.5)
WRITE(3,104)DMNS
104 FORMAT(5X," DELTA-  ",F15.5)
WRITE(3,105)R
105 FORMAT(5X," R  ",F15.5)
WRITE(3,107)BETA
107 FORMAT(5X," BETA  ",F15.5)
WRITE(3,202)
202 FORMAT(5X,"THE 3 ROTATIONAL FRICTIONAL RATIOS:")
WRITE(3,108)CA
108 FORMAT(5X," CA  ",F15.5)
WRITE(3,109)CB
109 FORMAT(5X," CB  ",F15.5)
WRITE(3,110)CC
110 FORMAT(5X," CC  ",F15.5)
WRITE(3,203)
203 FORMAT(5X,"THE 3 ROTATIONAL RELAXATION TIME RATIOS:")
WRITE(3,111)RHOA
111 FORMAT(5X," RHOA  ",F15.5)
WRITE(3,112)RHOB
112 FORMAT(5X," RHOB  ",F15.5)
WRITE(3,113)RHOC
113 FORMAT(5X," RHOC  ",F15.5)
WRITE(3,114)DELA
114 FORMAT(5X," DELTAA  ",F15.5)
WRITE(3,115)DELB
115 FORMAT(5X," DELTAB  ",F15.5)
WRITE(3,116)DELc
116 FORMAT(5X," DELTAC  ",F15.5)
WRITE(3,204)
204 FORMAT(5X,"THE HARMONIC MEAN RELAXATION TIME RATIO:")
WRITE(3,117)TAU
117 FORMAT(5X," TAU  ",F15.5)
WRITE(3,118)PSI
118 FORMAT(5X," PSI  ",F15.5)
WRITE(3,119)V
119 FORMAT(5X," LAMBDA  ",F15.5)
WRITE(3,120)GAMMAA
120 FORMAT(5X," GAMMAA  ",F15.5)
WRITE(3,121)GAMMAB
121 FORMAT(5X," GAMMAB  ",F15.5)
WRITE(3,122)GAMMAC
122 FORMAT(5X," GAMMAC  ",F15.5)
WRITE(3,123)MUA
123 FORMAT(5X," MUA  ",F15.5)
WRITE(3,124)MUB
124 FORMAT(5X," MUB  ",F15.5)
WRITE(3,125)MUC
125 FORMAT(5X," MUC  ",F15.5)
WRITE(3,126)GPLS
126 FORMAT(5X," GAMMA+  ",F15.5)
WRITE(3,127)GMNS
127 FORMAT(5X," GAMMA-  ",F15.5)
WRITE(3,201)

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201 FORMAT( 5X,"FLUORESCENCE ANISOTROPY RELAXATION TIME RATIOS:")
      WRITE(3,130)T1
130 FORMAT( 5X,"    T1    ",F15.5)
      WRITE(3,131)T2
131 FORMAT( 5X,"    T2    ",F15.5)
      WRITE(3,132)T3
132 FORMAT( 5X,"    T3    ",F15.5)
      WRITE(3,133)T4
133 FORMAT( 5X,"    T4    ",F15.5)
      WRITE(3,134)T5
134 FORMAT( 5X,"    T5    ",F15.5)
      STOP
      END

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REAL FUNCTION FUN(X)
COMMON/PARAM/A,C,NN
B=1.0
GOTO(10,20,30,40,50,60,70,80,90,100),NN
10 FUN=1/((A*A+X)**1.5*(B*B+X)**0.5*(C*C+X)**0.5)
      RETURN
20 FUN=1/((A*A+X)**0.5*(B*B+X)**1.5*(C*C+X)**0.5)
      RETURN
30 FUN=1/((A*A+X)**0.5*(B*B+X)**0.5*(C*C+X)**1.5)
      RETURN
40 FUN=1/((A*A+X)**0.5*(B*B+X)**1.5*(C*C+X)**1.5)
      RETURN
50 FUN=1/((A*A+X)**1.5*(B*B+X)**0.5*(C*C+X)**1.5)
      RETURN
60 FUN=1/((A*A+X)**1.5*(B*B+X)**1.5*(C*C+X)**0.5)
      RETURN
70 FUN=X/((A*A+X)**0.5*(B*B+X)**1.5*(C*C+X)**1.5)
      RETURN
80 FUN=X/((A*A+X)**1.5*(B*B+X)**0.5*(C*C+X)**1.5)
      RETURN
90 FUN=X/((A*A+X)**1.5*(B*B+X)**1.5*(C*C+X)**0.5)
      RETURN
100 FUN=1.0/(((A*A+X)*(B*B+X)*(C*C+X))**0.5)
      RETURN
      END

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Program 1 Results

A/B	1.50	B/C	1.50
NU	2.89170		
F	1.04410		
THE TA+	.16261		
THE TA-	.11622		
DELTA +	2.82127		
DELTA -	2.01645		
R	1.47887		
BETA	2.12334		
THE 3 ROTATIONAL FRICTIONAL RATIOS:			
CA	.89762		
CB	1.39800		
CC	1.47041		
THE 3 ROTATIONAL RELAXATION TIME RATIOS:			
RHOA	1.43329		
RHOB	1.11474		
RHOC	1.09327		
DELTAA	3.22152		
DELTAB	2.06846		
DELTAC	1.96660		
THE HARMONIC MEAN RELAXATION TIME RATIO:			
TAU	1.19548		
PSI	.98378		
LAMBDA	2.41886		
GAMMA A	.79414		
GAMMA AB	1.02107		
GAMMA AC	1.04112		
MUA	.92389		
MUB	1.07092		
MUC	1.08910		
GAMMA A+	1.11051		
GAMMA A-	.79372		
FLUORESCENCE ANISOTROPY RELAXATION TIME RATIOS:			
T1	1.02536		
T2	1.28883		
T3	1.31877		
T4	1.43405		
T5	1.02497		

Program 2

\*\*\*\*\*  
 THIS PROGRAM COMPUTES TABLES OF THE VISCOSITY INCREMENT NU,  
 THE TRANSLATIONAL FRICTIONAL RATIO (F/F0), THE ROTATIONAL  
 FRICTIONAL RATIOS (CA/C0, CB/C0, CC/C0), THE ROTATIONAL  
 RELAXATION TIME RATIOS (RHOA/RHO0, RHOB/RHO0, RHOC/RHO0), THE  
 HARMONIC MEAN RELAXATION TIME RATIO (TAU/TAU0), THE RIDGEWAY  
 ELECTRIC BIREFRINGENCE DECAY CONSTANTS (THETA+, THETA-), AND  
 THEIR CORRESPONDING SWELLING - INDEPENDENT FUNCTIONS:  
 R, BETA, DELTAA, DELTAB, DELTAC, GAMMAA, GAMMAB, GAMMAC,  
 MUA, MUB, MUC, PSI, DELTA+, DELTA-, GAMMA+ AND GAMMA-  
 AS FUNCTIONS OF THE AXIAL RATIOS A/B, B/C, IN THE RANGE 1.0 TO  
 2.0 IN STEPS OF 0.1, FOR A GENERAL TRIAXIAL ELLIPSOID PARTICLE  
 MODEL. (THE SUBSCRIPT "0" REFERS TO THE CORRESPONDING COEFFICIENT  
 FOR A SPHERE OF EQUAL VOLUME)  
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PROGRAM MAIN(INPUT,OUTPUT,TAPE2=INPUT,TAPE3=OUTPUT)
COMMON/PARAM/A,C,NN
EXTERNAL FUN
DIMENSION ALPHA(10,11,11),NU(11,11),F(11,11),R(11,11),H(1)
+,BETA(11,11),CA(11,11),CB(11,11),CC(11,11),M(11,11),O(11,11)
+,P(11,11),TPLS(11,11),TMNS(11,11),RHOA(11,11),RHOB(11,11)
+,RHOC(11,11),TAU(11,11),PSI(11,11),DELA(11,11),DELB(11,11)
+,DELc(11,11),GAMMAA(11,11),GAMMAB(11,11),GAMMAC(11,11),MUA(11,11)
+,MUB(11,11),MUC(11,11),DPLS(11,11),DMNS(11,11),GPLS(11,11)
+,GMNS(11,11),Y(11),Z(11),ZZ(11,11)
REAL NU,M,O,P,MUA,MUB,MUC,PSI
COMPUTE THE ELLIPTIC INTEGRALS
NN=0
D045 K=1,10
A=0.9
NN=NN+1
D040 I=1,11
A=A+0.1
C=1.0/0.9
D030 N=1,11
C=C/(1.0+0.1*C)
SET LIMITS FOR NUMERICAL INTEGRATION (THESE LIMITS
BELOW HAVE BEEN PREVIOUSLY TESTED FOR CONVERGENCE)
AA=0.0
BB=1000000
IF(NN.EQ.10) BB=500000000
MAXDIV=50
EPS=1.0E-08
ACC=0.0
IFAIL=0
CALL U.K. "NAG" LIBRARY ROUTINE FOR NUMERICAL EVALUATION
OF THE INTEGRALS "ALPHA" GIVEN IN THE SUBROUTINE BELOW
CALL D01AGF(AA,BB,FUN,MAXDIV,EPS,ACC,ANS,ERROR,NOFUN,IFAIL)
ALPHA(NN,I,N)=ANS
30 CONTINUE
40 CONTINUE
45 CONTINUE
B=1.0
A=0.9
D080 J=1,11
A=A+0.1
Y(J)=A
C=1.0/0.9
D070 N=1,11
C=C/(1.0+0.1*C)
Z(N)=1/C
NOW COMPUTE THE FUNCTION VALUES USING THE STORED INTEGRAL VALUES
NU(J,N)=(1.0/(A*B*C))*((4.0/15.0)*((ALPHA(7,J,N)+ALPHA(8,J,N)
+ +ALPHA(9,J,N))/(ALPHA(8,J,N)*ALPHA(9,J,N)+ALPHA(9,J,N)*ALPHA
+(7,J,N)+ALPHA(7,J,N)*ALPHA(8,J,N)))+(1.0/5.0)*(((ALPHA(2,J,N)
+ +ALPHA(3,J,N))/(ALPHA(4,J,N)*(B*B*ALPHA(2,J,N)+C*C*ALPHA(3,J,N)
+ ))+((ALPHA(3,J,N)+ALPHA(1,J,N))/(ALPHA(5,J,N)*(C*C*ALPHA(3,J,N)
+ +A*A*ALPHA(1,J,N))))+((ALPHA(1,J,N)+ALPHA(2,J,N))/(ALPHA(6,J,N)
+ *(A*A*ALPHA(1,J,N)+B*B*ALPHA(2,J,N))))))
F(J,N)=2.0*((A*B*C)**(1.0/3.0))*ALPHA(10,J,N))
R(J,N)=2.0*(1.0+(F(J,N)**3.0))/NU(J,N)
BETA(J,N)=(1.0/1000000.0)*((6.0249**1.0/3.0)*(10.0**23.0/3.0
+ ))/((16200.0*3.141592654*3.141592654)**(1.0/3.0))*(NU(J,N)
+ **(1.0/3.0))/F(J,N)
M(J,N)=(B*B+C*C)/(B*B*ALPHA(2,J,N)+C*C*ALPHA(3,J,N))
O(J,N)=(C*C+A*A)/(C*C*ALPHA(3,J,N)+A*A*ALPHA(1,J,N))
P(J,N)=(A*A+B*B)/(A*A*ALPHA(1,J,N)+B*B*ALPHA(2,J,N))
TPLS(J,N)=((A*B*C)/(12.0))*(((1.0/M(J,N))+(1.0/O(J,N))+(1.0/P(J,
+ N)))+((1.0/M(J,N)**2.0)+(1.0/O(J,N)**2.0)+(1.0/P(J,N)**2.0))-
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+ ((1.0/(M(J,N)*O(J,N)))+(1.0/(O(J,N)*P(J,N)))+(1.0/(P(J,N)*M(J,
+ N))))**0.5))
TMNS(J,N)=((A*B*C)/(12.0))*(((1.0/M(J,N))+(1.0/O(J,N))+(1.0/P(J,
+ N)))-((1.0/M(J,N)**2.0)+(1.0/O(J,N)**2.0)+(1.0/P(J,N)**2.0))-((1.0/(M(J,N)*O(J,N)))+(1.0/(O(J,N)*P(J,N)))+(1.0/(P(J,N)*M(J,
+ N))))**0.5))
CA(J,N)=(2.0/(3.0*A*B*C))*M(J,N)
CB(J,N)=(2.0/(3.0*A*B*C))*O(J,N)
CC(J,N)=(2.0/(3.0*A*B*C))*P(J,N)
RHOA(J,N)=2.0/((1.0/CB(J,N))+(1.0/CC(J,N)))
RHOB(J,N)=2.0/((1.0/CA(J,N))+(1.0/CC(J,N)))
RHOC(J,N)=2.0/((1.0/CA(J,N))+(1.0/CB(J,N)))
DELA(J,N)=NU(J,N)/CA(J,N)
DELB(J,N)=NU(J,N)/CB(J,N)
DELC(J,N)=NU(J,N)/CC(J,N)
TAU(J,N)=3.0/((1.0/CA(J,N))+(1.0/CB(J,N))+(1.0/CC(J,N)))
PSI(J,N)=F(J,N)*((1.0/TAU(J,N))**1.0/3.0)
ZZ(J,N)=(1.0/2.0)*(F(J,N)**3.0)
GAMMAA(J,N)=ZZ(J,N)*((1.0/CB(J,N))+(1.0/CC(J,N)))
GAMMAB(J,N)=ZZ(J,N)*((1.0/CA(J,N))+(1.0/CC(J,N)))
GAMMAC(J,N)=ZZ(J,N)*((1.0/CA(J,N))+(1.0/CB(J,N)))
MUA(J,N)=(CA(J,N)**1.0/3.0)/F(J,N)
MUB(J,N)=(CB(J,N)**1.0/3.0)/F(J,N)
MUC(J,N)=(CC(J,N)**1.0/3.0)/F(J,N)
DPLS(J,N)=6.0*TPLS(J,N)*NU(J,N)
DMNS(J,N)=6.0*TMNS(J,N)*NU(J,N)
GPLS(J,N)=6.0*TPLS(J,N)*(F(J,N)**3.0)
GMNS(J,N)=6.0*TMNS(J,N)*(F(J,N)**3.0)
70 CONTINUE
80 CONTINUE
C THE PROGRAM NOW WRITES OUT THE COMPUTED VALUES IN TABLE FORM
WRITE(3,600)
600 FORMAT(" ")
60 PRINT(3,60)
60 FORMAT("1 A/B B/C NU F/F0 R BETA")
6071 J=1,11
6072 N=1,11
WRITE(3,73)Y(J),Z(N),NU(J,N),F(J,N),R(J,N),BETA(J,N)
73 FORMAT(2F7.1,4F8.3)
72 CONTINUE
71 CONTINUE
WRITE(3,610)
610 FORMAT(" ")
61 PRINT(3,61)
61 FORMAT("1 A/B B/C CA/C0 CB/C0 CC/C0")
6074 J=1,11
6075 N=1,11
WRITE(3,76)Y(J),Z(N),CA(J,N),CB(J,N),CC(J,N)
76 FORMAT(2F7.1,3F8.3)
75 CONTINUE
74 CONTINUE
WRITE(3,620)
620 FORMAT(" ")
62 PRINT(3,62)
62 FORMAT("1 A/B B/C RHOA/RH00 RHOB/RH00 RHOC/RH00")
6081 J=1,11
6082 N=1,11
WRITE(3,83)Y(J),Z(N),RHOA(J,N),RHOB(J,N),RHOC(J,N)
83 FORMAT(2F7.1,3F9.3)
82 CONTINUE
81 CONTINUE
WRITE(3,630)
630 FORMAT(" ")
63 PRINT(3,63)
63 FORMAT("1 A/B B/C DELTA(A) DELTA(B) DELTA(C)")
6084 J=1,11
6085 N=1,11
WRITE(3,86)Y(J),Z(N),DELA(J,N),DELB(J,N),DELC(J,N)
86 FORMAT(2F7.1,3F8.3)
85 CONTINUE
84 CONTINUE
WRITE(3,640)
640 FORMAT(" ")
64 PRINT(3,64)
64 FORMAT("1 A/B B/C GAMMA(A) GAMMA(B) GAMMA(C)")
6091 J=1,11
6092 N=1,11
WRITE(3,93)Y(J),Z(N),GAMMAA(J,N),GAMMAB(J,N),GAMMAC(J,N)
93 FORMAT(2F7.1,3F8.3)
92 CONTINUE
91 CONTINUE

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      WRITE(3,650)
650  FORMAT(  "  ")
      PRINT(3,65)
65  FORMAT( "1      A/B      B/C      MU(A)      MU(B)      MU(C)" )
      DO94 J=1,11
      DO95 N=1,11
      WRITE(3,96)Y(J),Z(N),MUA(J,N),MUB(J,N),MUC(J,N)
96  FORMAT( 2F7.1,3F8.3)
95  CONTINUE
94  CONTINUE
      WRITE(3,660)
660  FORMAT(  "  ")
      PRINT(3,66)
66  FORMAT( "1      A/B      B/C      THETA+      THETA-      TAU/TAU0      PSI")
      DO101 J=1,11
      DO102 N=1,11
      WRITE(3,103)Y(J),Z(N),TPLS(J,N),TMNS(J,N),TAU(J,N),PSI(J,N)
103 FORMAT( 2F7.1,4F8.3)
102 CONTINUE
101 CONTINUE
      WRITE(3,670)
670  FORMAT(  "  ")
      PRINT(3,67)
67  FORMAT( "1      A/B      B/C      DELTA+      DELTA-")
      DO104 J=1,11
      DO105 N=1,11
      WRITE(3,106)Y(J),Z(N),DPLS(J,N),DMNS(J,N)
106 FORMAT( 2F7.1,2F8.3)
105 CONTINUE
104 CONTINUE
      WRITE(3,680)
680  FORMAT(  "  ")
      PRINT(3,68)
68  FORMAT( "1      A/B      B/C      GAMMA+      GAMMA-")
      DO111 J=1,11
      DO112 N=1,11
      WRITE(3,113)Y(J),Z(N),GPLS(J,N),GMNS(J,N)
113 FORMAT( 2F7.1,2F8.3)
112 CONTINUE
111 CONTINUE
      WRITE(3,690)
690  FORMAT(  "  ")
      DO114 J=1,11
      DO115 N=1,11
115 CONTINUE
114 CONTINUE
      STOP
      END

```

CCC

```

REAL FUNCTION FUN(X)
COMMON/PARAM/A,C,NN
B=1.0
GOTO(10,20,30,40,50,60,70,80,90,100),NN
10 FUN=1/((A*A+X)**1.5*(B*B+X)**0.5*(C*C+X)**0.5)
      RETURN
20 FUN=1/((A*A+X)**0.5*(B*B+X)**1.5*(C*C+X)**0.5)
      RETURN
30 FUN=1/((A*A+X)**0.5*(B*B+X)**0.5*(C*C+X)**1.5)
      RETURN
40 FUN=1/((A*A+X)**0.5*(B*B+X)**1.5*(C*C+X)**1.5)
      RETURN
50 FUN=1/((A*A+X)**1.5*(B*B+X)**0.5*(C*C+X)**1.5)
      RETURN
60 FUN=1/((A*A+X)**1.5*(B*B+X)**1.5*(C*C+X)**0.5)
      RETURN
70 FUN=X/((A*A+X)**0.5*(B*B+X)**1.5*(C*C+X)**1.5)
      RETURN
80 FUN=X/((A*A+X)**1.5*(B*B+X)**0.5*(C*C+X)**1.5)
      RETURN
90 FUN=X/((A*A+X)**1.5*(B*B+X)**1.5*(C*C+X)**0.5)
      RETURN
100 FUN=1.0/(((A*A+X)*(B*B+X)*(C*C+X))**0.5)
      RETURN
      END

```

A/B	B/C	NU	F/F0	R	BETA
1.0	1.0	2.500	1.000	1.600	2.112
1.0	1.1	2.507	1.001	1.598	2.112
1.0	1.2	2.524	1.003	1.592	2.113
1.0	1.3	2.531	1.006	1.583	2.113
1.0	1.4	2.538	1.010	1.572	2.114
1.0	1.5	2.542	1.014	1.560	2.115
1.0	1.6	2.546	1.019	1.548	2.115
1.0	1.7	2.550	1.025	1.534	2.116
1.0	1.8	2.553	1.030	1.521	2.117
1.0	1.9	2.557	1.036	1.507	2.118
1.0	2.0	2.561	1.042	1.493	2.118
1.1	1.0	2.567	1.001	1.598	2.112
1.1	1.1	2.570	1.002	1.593	2.112
1.1	1.2	2.574	1.005	1.585	2.113
1.1	1.3	2.576	1.009	1.574	2.114
1.1	1.4	2.576	1.014	1.562	2.115
1.1	1.5	2.576	1.019	1.549	2.115
1.1	1.6	2.576	1.024	1.535	2.116
1.1	1.7	2.576	1.030	1.521	2.117
1.1	1.8	2.576	1.036	1.507	2.118
1.1	1.9	2.577	1.042	1.492	2.119
1.1	2.0	2.583	1.049	1.478	2.120
1.2	1.0	2.583	1.003	1.591	2.113
1.2	1.1	2.584	1.005	1.584	2.113
1.2	1.2	2.585	1.009	1.574	2.114
1.2	1.3	2.585	1.013	1.562	2.115
1.2	1.4	2.585	1.018	1.549	2.116
1.2	1.5	2.585	1.024	1.535	2.117
1.2	1.6	2.585	1.030	1.520	2.118
1.2	1.7	2.585	1.036	1.505	2.119
1.2	1.8	2.585	1.043	1.490	2.120
1.2	1.9	2.587	1.049	1.475	2.120
1.2	2.0	2.591	1.056	1.460	2.121
1.3	1.0	2.591	1.006	1.582	2.114
1.3	1.1	2.592	1.009	1.573	2.114
1.3	1.2	2.592	1.013	1.561	2.115
1.3	1.3	2.592	1.018	1.547	2.116
1.3	1.4	2.592	1.024	1.533	2.118
1.3	1.5	2.592	1.030	1.520	2.119
1.3	1.6	2.592	1.036	1.505	2.120
1.3	1.7	2.592	1.043	1.490	2.120
1.3	1.8	2.592	1.049	1.475	2.120
1.3	1.9	2.593	1.056	1.460	2.121
1.3	2.0	2.593	1.064	1.582	2.114
1.4	1.0	2.593	1.006	1.573	2.114
1.4	1.1	2.593	1.009	1.561	2.115
1.4	1.2	2.593	1.013	1.547	2.116
1.4	1.3	2.593	1.018	1.533	2.118
1.4	1.4	2.593	1.024	1.520	2.119
1.4	1.5	2.593	1.030	1.505	2.120
1.4	1.6	2.593	1.036	1.490	2.120
1.4	1.7	2.593	1.043	1.475	2.120
1.4	1.8	2.593	1.049	1.460	2.121
1.4	1.9	2.594	1.056	1.582	2.114
1.4	2.0	2.594	1.064	1.573	2.114
1.5	1.0	2.594	1.006	1.561	2.115
1.5	1.1	2.594	1.009	1.547	2.116
1.5	1.2	2.594	1.013	1.533	2.118
1.5	1.3	2.594	1.018	1.520	2.119
1.5	1.4	2.594	1.024	1.505	2.120
1.5	1.5	2.594	1.030	1.490	2.120
1.5	1.6	2.594	1.036	1.475	2.120
1.5	1.7	2.594	1.043	1.460	2.121
1.5	1.8	2.594	1.049	1.582	2.114
1.5	1.9	2.595	1.056	1.573	2.114
1.5	2.0	2.595	1.064	1.561	2.115
1.6	1.0	2.595	1.006	1.547	2.116
1.6	1.1	2.595	1.009	1.533	2.118
1.6	1.2	2.595	1.013	1.520	2.119
1.6	1.3	2.595	1.018	1.505	2.120
1.6	1.4	2.595	1.024	1.490	2.120
1.6	1.5	2.595	1.030	1.475	2.120
1.6	1.6	2.595	1.036	1.460	2.121
1.6	1.7	2.595	1.043	1.582	2.114
1.6	1.8	2.595	1.049	1.573	2.114
1.6	1.9	2.596	1.056	1.561	2.115
1.6	2.0	2.596	1.064	1.547	2.116
1.7	1.0	2.596	1.006	1.533	2.118
1.7	1.1	2.596	1.009	1.520	2.119
1.7	1.2	2.596	1.013	1.505	2.120
1.7	1.3	2.596	1.018	1.490	2.120
1.7	1.4	2.596	1.024	1.475	2.120
1.7	1.5	2.596	1.030	1.460	2.121
1.7	1.6	2.596	1.036	1.582	2.114
1.7	1.7	2.596	1.043	1.573	2.114
1.7	1.8	2.596	1.049	1.561	2.115
1.7	1.9	2.597	1.056	1.547	2.116
1.7	2.0	2.597	1.064	1.533	2.118
1.8	1.0	2.597	1.006	1.520	2.119
1.8	1.1	2.597	1.009	1.505	2.120
1.8	1.2	2.597	1.013	1.490	2.120
1.8	1.3	2.597	1.018	1.475	2.120
1.8	1.4	2.597	1.024	1.460	2.121
1.8	1.5	2.597	1.030	1.582	2.114
1.8	1.6	2.597	1.036	1.573	2.114
1.8	1.7	2.597	1.043	1.561	2.115
1.8	1.8	2.597	1.049	1.547	2.116
1.8	1.9	2.598	1.056	1.533	2.118
1.8	2.0	2.598	1.064	1.520	2.119
1.9	1.0	2.598	1.006	1.505	2.120
1.9	1.1	2.598	1.009	1.490	2.120
1.9	1.2	2.598	1.013	1.475	2.120
1.9	1.3	2.598	1.018	1.460	2.121
1.9	1.4	2.598	1.024	1.582	2.114
1.9	1.5	2.598	1.030	1.573	2.114
1.9	1.6	2.598	1.036	1.561	2.115
1.9	1.7	2.598	1.043	1.547	2.116
1.9	1.8	2.598	1.049	1.533	2.118
1.9	1.9	2.599	1.056	1.520	2.119
1.9	2.0	2.599	1.064	1.505	2.120
2.0	1.0	2.599	1.006	1.490	2.120
2.0	1.1	2.599	1.009	1.475	2.120
2.0	1.2	2.599	1.013	1.460	2.121
2.0	1.3	2.599	1.018	1.582	2.114
2.0	1.4	2.599	1.024	1.573	2.114
2.0	1.5	2.599	1.030	1.561	2.115
2.0	1.6	2.599	1.036	1.547	2.116
2.0	1.7	2.599	1.043	1.533	2.118
2.0	1.8	2.599	1.049	1.520	2.119
2.0	1.9	2.600	1.056	1.505	2.120
2.0	2.0	2.600	1.064	1.490	2.120
2.1	1.0	2.600	1.006	1.475	2.123
2.1	1.1	2.600	1.009	1.460	2.125
2.1	1.2	2.600	1.013	1.582	2.112
2.1	1.3	2.600	1.018	1.573	2.112
2.1	1.4	2.600	1.024	1.561	2.113
2.1	1.5	2.600	1.030	1.547	2.115
2.1	1.6	2.600	1.036	1.533	2.116
2.1	1.7	2.600	1.043	1.520	2.117
2.1	1.8	2.600	1.049	1.505	2.118
2.1	1.9	2.601	1.056	1.490	2.119
2.1	2.0	2.601	1.064	1.475	2.120
2.2	1.0	2.601	1.006	1.460	2.122
2.2	1.1	2.601	1.009	1.444	2.124
2.2	1.2	2.601	1.013	1.437	2.126
2.2	1.3	2.601	1.018	1.455	2.128
2.2	1.4	2.601	1.024	1.437	2.129
2.2	1.5	2.601	1.030	1.419	2.131

1.7	1.7	3.204	1.076	1.402	2.132
1.7	1.8	3.285	1.084	1.384	2.134
1.7	1.9	3.368	1.092	1.368	2.135
1.7	2.0	3.453	1.101	1.352	2.137
1.8	1.8	2.785	1.031	1.506	2.123
1.8	1.9	2.842	1.037	1.490	2.125
1.8	2.0	2.907	1.044	1.472	2.127
1.8	2.1	2.978	1.052	1.453	2.129
1.8	2.2	3.053	1.059	1.434	2.131
1.8	2.3	3.132	1.068	1.415	2.133
1.8	2.4	3.215	1.076	1.397	2.134
1.8	2.5	3.300	1.085	1.379	2.136
1.8	2.6	3.386	1.093	1.362	2.138
1.8	2.7	3.475	1.102	1.345	2.139
1.8	2.8	3.565	1.111	1.329	2.141
1.9	1.9	2.844	1.038	1.489	2.125
1.9	2.0	2.908	1.044	1.471	2.127
1.9	2.1	2.978	1.051	1.452	2.130
1.9	2.2	3.055	1.059	1.432	2.132
1.9	2.3	3.137	1.067	1.413	2.134
1.9	2.4	3.222	1.076	1.394	2.136
1.9	2.5	3.310	1.085	1.375	2.138
1.9	2.6	3.400	1.093	1.357	2.140
1.9	2.7	3.492	1.102	1.340	2.142
1.9	2.8	3.586	1.111	1.323	2.143
1.9	2.9	3.681	1.120	1.307	2.145
2.0	2.0	2.908	1.044	1.470	2.128
2.0	2.1	2.977	1.051	1.451	2.133
2.0	2.2	3.054	1.059	1.432	2.135
2.0	2.3	3.137	1.067	1.412	2.138
2.0	2.4	3.224	1.075	1.392	2.140
2.0	2.5	3.315	1.084	1.372	2.142
2.0	2.6	3.408	1.093	1.354	2.144
2.0	2.7	3.504	1.102	1.335	2.146
2.0	2.8	3.602	1.112	1.318	2.148
2.0	2.9	3.702	1.121	1.301	2.149
2.0	3.0	3.803	1.130	1.285	2.149

A/B	B/C	CA/C0	CB/C0	CC/C0
1.0	1.0	1.000	1.000	1.000
1.0	1.1	.986	.986	1.040
1.0	1.2	.983	.983	1.081
1.0	1.3	.988	.988	1.121
1.0	1.4	.998	.998	1.162
1.0	1.5	1.013	1.013	1.203
1.0	1.6	1.032	1.032	1.244
1.0	1.7	1.054	1.054	1.286
1.0	1.8	1.078	1.078	1.327
1.0	1.9	1.104	1.104	1.368
1.0	2.0	1.132	1.132	1.410
1.1	1.0	.964	1.025	1.025
1.1	1.1	.952	1.026	1.067
1.1	1.2	.950	1.038	1.110
1.1	1.3	.955	1.056	1.153
1.1	1.4	.966	1.078	1.196
1.1	1.5	.981	1.103	1.240
1.1	1.6	1.000	1.132	1.283
1.1	1.7	1.021	1.162	1.327
1.1	1.8	1.045	1.195	1.370
1.1	1.9	1.071	1.229	1.414
1.1	2.0	1.099	1.058	1.458
1.2	1.0	.934	1.062	1.058
1.2	1.1	.923	1.075	1.103
1.2	1.2	.922	1.095	1.148
1.2	1.3	.928	1.120	1.194
1.2	1.4	.939	1.150	1.240
1.2	1.5	.955	1.182	1.286
1.2	1.6	.973	1.217	1.332
1.2	1.7	.995	1.254	1.378
1.2	1.8	1.019	1.293	1.425
1.2	1.9	1.044	1.333	1.471
1.2	2.0	1.072	1.097	1.518
1.3	1.0	.909	1.110	1.097
1.3	1.1	.899	1.131	1.146
1.3	1.2	.899	1.159	1.194
1.3	1.3	.905	1.191	1.243
1.3	1.4	.917	1.227	1.292
1.3	1.5	.933	1.266	1.341
1.3	1.6	.951	1.308	1.390
1.3	1.7	.973	1.351	1.439
1.3	1.8	.997	1.397	1.488
1.3	1.9	1.022	1.443	1.538
1.3	2.0	1.049	1.443	1.587
1.4	1.0	.887	1.143	1.143
1.4	1.1	.879	1.164	1.194
1.4	1.2	.879	1.193	1.246
1.4	1.3	.886	1.228	1.298
1.4	1.4	.898	1.267	1.350
1.4	1.5	.914	1.310	1.402
1.4	1.6	.933	1.356	1.455
1.4	1.7	.954	1.404	1.507
1.4	1.8	.978	1.454	1.560
1.4	1.9	1.003	1.506	1.612
1.4	2.0	1.030	1.559	1.665
1.5	1.0	.869	1.193	1.193
1.5	1.1	.862	1.222	1.248
1.5	1.2	.862	1.259	1.304
1.5	1.3	.870	1.301	1.359
1.5	1.4	.882	1.348	1.415
1.5	1.5	.898	1.398	1.470
1.5	1.6	.917	1.451	1.526
1.5	1.7	.938	1.506	1.582
1.5	1.8	.961	1.563	1.638
1.5	1.9	.987	1.621	1.694
1.5	2.0	1.013	1.681	1.751
1.6	1.0	.853	1.248	1.248
1.6	1.1	.846	1.285	1.307
1.6	1.2	.848	1.330	1.366
1.6	1.3	.855	1.379	1.425
1.6	1.4	.868	1.433	1.485
1.6	1.5	.884	1.490	1.544
1.6	1.6	.903	1.550	1.604
1.6	1.7	.924	1.612	1.663
1.6	1.8	.947	1.676	1.723
1.6	1.9	.972	1.741	1.783
1.6	2.0	.999	1.807	1.843
1.7	1.0	.839	1.307	1.307
1.7	1.1	.833	1.352	1.370
1.7	1.2	.835	1.404	1.433
1.7	1.3	.843	1.461	1.496
1.7	1.4	.855	1.523	1.559
1.7	1.5	.871	1.587	1.623
1.7	1.6	.890	1.654	1.686

1.7	1.7	.912	1.723	1.750
1.7	1.8	.935	1.793	1.814
1.7	1.9	.960	1.865	1.877
1.7	2.0	.986	1.939	1.941
1.8	1.0	.827	1.370	1.370
1.8	1.1	.822	1.423	1.437
1.8	1.2	.824	1.483	1.504
1.8	1.3	.832	1.547	1.571
1.8	1.4	.845	1.616	1.639
1.8	1.5	.861	1.687	1.706
1.8	1.6	.880	1.762	1.774
1.8	1.7	.901	1.838	1.842
1.8	1.8	.924	1.915	1.918
1.8	1.9	.949	1.995	1.978
1.8	2.0	.975	2.075	2.046
1.9	1.0	.816	1.436	1.436
1.9	1.1	.811	1.497	1.507
1.9	1.2	.814	1.564	1.579
1.9	1.3	.822	1.637	1.650
1.9	1.4	.835	1.713	1.722
1.9	1.5	.851	1.792	1.794
1.9	1.6	.870	1.873	1.866
1.9	1.7	.892	1.957	1.938
1.9	1.8	.915	2.042	2.011
1.9	1.9	.939	2.128	2.083
1.9	2.0	.965	2.216	2.155
2.0	1.0	.807	1.505	1.505
2.0	1.1	.802	1.574	1.581
2.0	1.2	.805	1.650	1.657
2.0	1.3	.814	1.730	1.733
2.0	1.4	.826	1.813	1.810
2.0	1.5	.843	1.900	1.886
2.0	1.6	.862	1.989	1.963
2.0	1.7	.883	2.080	2.040
2.0	1.8	.906	2.172	2.116
2.0	1.9	.931	2.266	2.193
2.0	2.0	.957	2.361	2.270

A/B	B/C	RHOA/RHO0	RHOB/RHO0	RHOC/RHO0
1.0	1.0	1.000	1.000	1.000
1.0	1.1	1.013	1.013	.986
1.0	1.2	1.030	1.030	.983
1.0	1.3	1.050	1.050	.988
1.0	1.4	1.074	1.074	.998
1.0	1.5	1.100	1.100	1.013
1.0	1.6	1.128	1.128	1.032
1.0	1.7	1.158	1.158	1.054
1.0	1.8	1.189	1.189	1.078
1.0	1.9	1.222	1.222	1.104
1.0	2.0	1.256	1.256	1.132
1.1	1.0	1.025	.993	.993
1.1	1.1	1.043	1.006	.985
1.1	1.2	1.066	1.024	.986
1.1	1.3	1.092	1.045	.995
1.1	1.4	1.122	1.069	1.009
1.1	1.5	1.153	1.095	1.027
1.1	1.6	1.187	1.124	1.049
1.1	1.7	1.222	1.154	1.074
1.1	1.8	1.258	1.186	1.101
1.1	1.9	1.295	1.219	1.130
1.1	2.0	1.334	1.253	1.160
1.2	1.0	1.058	.992	.992
1.2	1.1	1.082	1.005	.988
1.2	1.2	1.111	1.023	.993
1.2	1.3	1.143	1.044	1.005
1.2	1.4	1.177	1.069	1.022
1.2	1.5	1.214	1.096	1.043
1.2	1.6	1.253	1.125	1.068
1.2	1.7	1.293	1.156	1.095
1.2	1.8	1.334	1.188	1.124
1.2	1.9	1.376	1.222	1.155
1.2	2.0	1.419	1.256	1.188
1.3	1.0	1.097	.994	.994
1.3	1.1	1.128	1.008	1.002
1.3	1.2	1.162	1.026	1.017
1.3	1.3	1.199	1.048	1.036
1.3	1.4	1.239	1.072	1.060
1.3	1.5	1.281	1.100	1.086
1.3	1.6	1.325	1.130	1.116
1.3	1.7	1.370	1.161	1.147
1.3	1.8	1.417	1.194	1.180
1.3	1.9	1.464	1.228	1.215
1.4	2.0	1.512	1.263	.999
1.4	1.0	1.143	.999	1.002
1.4	1.1	1.179	1.013	1.012
1.4	1.2	1.219	1.031	1.029
1.4	1.3	1.262	1.053	1.051
1.4	1.4	1.307	1.079	1.077
1.4	1.5	1.355	1.107	1.105
1.4	1.6	1.404	1.137	1.136
1.4	1.7	1.454	1.168	1.169
1.4	1.8	1.505	1.202	1.204
1.4	1.9	1.558	1.237	1.240
1.5	2.0	1.611	1.272	1.272
1.5	1.0	1.193	1.006	1.006
1.5	1.1	1.235	1.020	1.011
1.5	1.2	1.281	1.038	1.024
1.5	1.3	1.330	1.061	1.043
1.5	1.4	1.381	1.086	1.066
1.5	1.5	1.433	1.115	1.093
1.5	1.6	1.488	1.145	1.123
1.5	1.7	1.543	1.178	1.156
1.5	1.8	1.600	1.212	1.190
1.5	1.9	1.657	1.247	1.227
1.5	2.0	1.715	1.283	1.264
1.6	1.0	1.248	1.014	1.014
1.6	1.1	1.296	1.028	1.021
1.6	1.2	1.348	1.046	1.035
1.6	1.3	1.402	1.069	1.056
1.6	1.4	1.458	1.095	1.081
1.6	1.5	1.517	1.124	1.109
1.6	1.6	1.576	1.155	1.141
1.6	1.7	1.637	1.188	1.175
1.6	1.8	1.699	2.223	1.210
1.6	1.9	1.762	1.258	1.248
1.6	2.0	1.825	1.295	1.287
1.7	1.0	1.307	1.022	1.022
1.7	1.1	1.361	1.036	1.031
1.7	1.2	1.413	1.055	1.047
1.7	1.3	1.479	1.078	1.069
1.7	1.4	1.541	1.105	1.095
1.7	1.5	1.605	1.134	1.125
1.7	1.6	1.670	1.165	1.158

1.7	1.7	1.736	1.199	1.192
1.7	1.8	1.803	1.234	1.229
1.7	1.9	1.871	1.270	1.268
1.7	2.0	1.940	1.308	1.307
1.8	1.0	1.370	1.032	1.032
1.8	1.1	1.430	1.045	1.042
1.8	1.2	1.493	1.065	1.059
1.8	1.3	1.559	1.088	1.082
1.8	1.4	1.627	1.115	1.109
1.8	1.5	1.697	1.144	1.140
1.8	1.6	1.768	1.176	1.173
1.8	1.7	1.840	1.210	1.209
1.8	1.8	1.913	1.246	1.247
1.8	1.9	1.986	1.283	1.286
1.8	2.0	2.060	1.321	1.327
1.9	1.0	1.436	1.041	1.041
1.9	1.1	1.502	1.055	1.052
1.9	1.2	1.572	1.074	1.071
1.9	1.3	1.644	1.098	1.095
1.9	1.4	1.718	1.125	1.123
1.9	1.5	1.793	1.155	1.154
1.9	1.6	1.870	1.187	1.188
1.9	1.7	1.948	1.221	1.225
1.9	1.8	2.026	1.257	1.263
1.9	1.9	2.105	1.295	1.303
1.9	2.0	2.185	1.334	1.345
2.0	1.0	1.505	1.050	1.050
2.0	1.1	1.577	1.064	1.063
2.0	1.2	1.653	1.084	1.082
2.0	1.3	1.731	1.107	1.107
2.0	1.4	1.812	1.135	1.135
2.0	1.5	1.893	1.165	1.168
2.0	1.6	1.976	1.198	1.203
2.0	1.7	2.059	1.233	1.240
2.0	1.8	2.144	1.269	1.279
2.0	1.9	2.229	1.307	1.320
2.0	2.0	2.314	1.346	1.362

A/B	B/C	DELTA (A)	DELTA (B)	DELTA (C)
1.0	1.0	2.500	2.500	2.500
1.0	1.1	2.541	2.541	2.410
1.0	1.2	2.568	2.568	2.336
1.0	1.3	2.582	2.582	2.274
1.0	1.4	2.588	2.588	2.222
1.0	1.5	2.586	2.586	2.178
1.0	1.6	2.579	2.579	2.139
1.0	1.7	2.568	2.568	2.105
1.0	1.8	2.555	2.555	2.075
1.0	1.9	2.539	2.539	2.048
1.0	2.0	2.522	2.522	2.024
1.1	1.0	2.601	2.446	2.446
1.1	1.1	2.648	2.470	2.362
1.1	1.2	2.679	2.481	2.292
1.1	1.3	2.697	2.482	2.234
1.1	1.4	2.706	2.475	2.185
1.1	1.5	2.707	2.464	2.143
1.1	1.6	2.702	2.449	2.106
1.1	1.7	2.694	2.431	2.074
1.1	1.8	2.682	2.412	2.046
1.1	1.9	2.667	2.392	2.020
1.1	2.0	2.651	2.371	1.998
1.2	1.0	2.704	2.387	2.387
1.2	1.1	2.757	2.397	2.308
1.2	1.2	2.793	2.395	2.242
1.2	1.3	2.815	2.385	2.188
1.2	1.4	2.827	2.370	2.141
1.2	1.5	2.831	2.351	2.102
1.2	1.6	2.829	2.330	2.067
1.2	1.7	2.822	2.308	2.037
1.2	1.8	2.812	2.285	2.010
1.2	1.9	2.799	2.261	1.987
1.2	2.0	2.784	2.238	1.966
1.3	1.0	2.809	2.326	2.326
1.3	1.1	2.868	2.323	2.251
1.3	1.2	2.909	2.311	2.190
1.3	1.3	2.936	2.293	2.139
1.3	1.4	2.951	2.272	2.095
1.3	1.5	2.958	2.248	2.058
1.3	1.6	2.959	2.223	2.025
1.3	1.7	2.954	2.197	1.997
1.3	1.8	2.945	2.172	1.972
1.3	1.9	2.934	2.147	1.950
1.3	2.0	2.920	2.122	1.930
1.4	1.0	2.916	2.264	2.264
1.4	1.1	2.981	2.252	2.194
1.4	1.2	3.028	2.232	2.136
1.4	1.3	3.059	2.208	2.088
1.4	1.4	3.078	2.181	2.047
1.4	1.5	3.088	2.154	2.012
1.4	1.6	3.091	2.126	1.982
1.4	1.7	3.089	2.099	1.955
1.4	1.8	3.082	2.072	1.932
1.4	1.9	3.072	2.046	1.911
1.4	2.0	3.060	2.021	1.892
1.5	1.0	3.026	2.203	2.203
1.5	1.1	3.097	2.183	2.137
1.5	1.2	3.149	2.157	2.083
1.5	1.3	3.185	2.128	2.038
1.5	1.4	3.208	2.098	2.000
1.5	1.5	3.222	2.068	1.967
1.5	1.6	3.227	2.039	1.938
1.5	1.7	3.222	2.015	1.913
1.5	1.8	3.222	1.983	1.891
1.5	1.9	3.214	1.956	1.871
1.5	2.0	3.204	1.931	1.854
1.6	1.0	3.137	2.144	2.144
1.6	1.1	3.215	2.117	2.082
1.6	1.2	3.273	2.087	2.031
1.6	1.3	3.313	2.055	1.989
1.6	1.4	3.341	2.023	1.953
1.6	1.5	3.358	1.991	1.922
1.6	1.6	3.366	1.960	1.895
1.6	1.7	3.369	1.931	1.871
1.6	1.8	3.366	1.903	1.851
1.6	1.9	3.360	1.877	1.832
1.6	2.0	3.351	1.852	1.816
1.7	1.0	3.251	2.055	2.087
1.7	1.1	3.336	2.021	2.029
1.7	1.2	3.399	1.987	1.981
1.7	1.3	3.445	1.953	1.941
1.7	1.4	3.476	1.920	1.907
1.7	1.5	3.497	1.889	1.878
1.7	1.6	3.509	1.889	1.853

1.7	1.7	3.514	1.860	1.831
1.7	1.8	3.513	1.832	1.811
1.7	1.9	3.509	1.806	1.794
1.7	2.0	3.501	1.781	1.779
1.8	1.0	3.366	2.033	2.033
1.8	1.1	3.459	1.997	1.978
1.8	1.2	3.528	1.960	1.933
1.8	1.3	3.579	1.924	1.895
1.8	1.4	3.615	1.889	1.863
1.8	1.5	3.639	1.856	1.836
1.8	1.6	3.654	1.825	1.812
1.8	1.7	3.662	1.796	1.792
1.8	1.8	3.664	1.768	1.773
1.8	1.9	3.661	1.742	1.757
1.8	2.0	3.655	1.718	1.743
1.9	1.0	3.484	1.981	1.981
1.9	1.1	3.584	1.942	1.929
1.9	1.2	3.660	1.904	1.887
1.9	1.3	3.716	1.867	1.851
1.9	1.4	3.757	1.831	1.821
1.9	1.5	3.785	1.798	1.796
1.9	1.6	3.803	1.767	1.773
1.9	1.7	3.813	1.738	1.754
1.9	1.8	3.818	1.710	1.737
1.9	1.9	3.817	1.685	1.722
1.9	2.0	3.813	1.662	1.708
2.0	1.0	3.604	1.932	1.932
2.0	1.1	3.712	1.891	1.883
2.0	1.2	3.794	1.851	1.843
2.0	1.3	3.856	1.814	1.810
2.0	1.4	3.901	1.778	1.781
2.0	1.5	3.933	1.745	1.757
2.0	1.6	3.955	1.714	1.736
2.0	1.7	3.968	1.685	1.718
2.0	1.8	3.975	1.658	1.702
2.0	1.9	3.977	1.634	1.688
2.0	2.0	3.975	1.611	1.675

A/B	B/C	GAMMA(A)	GAMMA(B)	GAMMA(C)
1.0	1.0	1.000	1.000	1.000
1.0	1.1	.990	.990	1.016
1.0	1.2	.980	.980	1.026
1.0	1.3	.970	.970	1.031
1.0	1.4	.959	.959	1.032
1.0	1.5	.949	.949	1.031
1.0	1.6	.939	.939	1.027
1.0	1.7	.929	.929	1.021
1.0	1.8	.919	.919	1.015
1.0	1.9	.910	.910	1.008
1.0	2.0	.901	.901	1.000
1.1	1.0	.978	1.009	1.009
1.1	1.1	.966	1.001	1.023
1.1	1.2	.953	.993	1.030
1.1	1.3	.941	.984	1.033
1.1	1.4	.929	.974	1.032
1.1	1.5	.917	.965	1.029
1.1	1.6	.905	.956	1.024
1.1	1.7	.894	.947	1.017
1.1	1.8	.884	.937	1.010
1.1	1.9	.874	.929	1.002
1.1	2.0	.864	.920	.994
1.2	1.0	.954	1.017	1.017
1.2	1.1	.939	1.011	1.029
1.2	1.2	.925	1.004	1.034
1.2	1.3	.911	.996	1.036
1.2	1.4	.897	.988	1.034
1.2	1.5	.885	.980	1.029
1.2	1.6	.872	.971	1.023
1.2	1.7	.861	.963	1.016
1.2	1.8	.850	.954	1.008
1.2	1.9	.840	.946	1.000
1.2	2.0	.830	.938	.991
1.3	1.0	.928	1.025	1.025
1.3	1.1	.912	1.020	1.035
1.3	1.2	.896	1.015	1.039
1.3	1.3	.881	1.008	1.039
1.3	1.4	.867	1.001	1.036
1.3	1.5	.853	.994	1.031
1.3	1.6	.840	.986	1.025
1.3	1.7	.829	.978	1.018
1.3	1.8	.817	.970	1.009
1.3	1.9	.807	.962	1.001
1.3	2.0	.797	.954	.992
1.4	1.0	.902	1.032	1.032
1.4	1.1	.884	1.029	1.041
1.4	1.2	.867	1.025	1.044
1.4	1.3	.851	1.020	1.044
1.4	1.4	.837	1.014	1.041
1.4	1.5	.823	1.007	1.035
1.4	1.6	.810	1.000	1.029
1.4	1.7	.798	.993	1.021
1.4	1.8	.787	.986	1.013
1.4	1.9	.777	.978	1.005
1.4	2.0	.767	.971	.996
1.5	1.0	.876	1.039	1.039
1.5	1.1	.857	1.038	1.047
1.5	1.2	.839	1.036	1.050
1.5	1.3	.823	1.032	1.050
1.5	1.4	.808	1.027	1.046
1.5	1.5	.794	1.021	1.041
1.5	1.6	.781	1.015	1.035
1.5	1.7	.769	1.008	1.027
1.5	1.8	.758	1.001	1.019
1.5	1.9	.748	.994	1.011
1.5	2.0	.739	.987	1.002
1.6	1.0	.850	1.047	1.047
1.6	1.1	.831	1.048	1.055
1.6	1.2	.813	1.047	1.058
1.6	1.3	.796	1.044	1.057
1.6	1.4	.781	1.040	1.054
1.6	1.5	.767	1.035	1.048
1.6	1.6	.754	1.029	1.042
1.6	1.7	.742	1.023	1.035
1.6	1.8	.731	1.017	1.027
1.6	1.9	.721	1.010	1.019
1.6	2.0	.712	1.003	1.010
1.7	1.0	.825	.955	1.055
1.7	1.1	.805	.958	1.063
1.7	1.2	.787	.958	1.066
1.7	1.3	.770	.956	1.065
1.7	1.4	.755	.953	1.062
1.7	1.5	.741	.949	1.057
1.7	1.6	.729	1.044	1.051

1.7	1.7	.717	1.038	1.044
1.7	1.8	.706	1.032	1.036
1.7	1.9	.697	1.026	1.029
1.7	2.0	.688	1.020	1.020
1.8	1.0	.801	1.064	1.064
1.8	1.1	.781	1.068	1.072
1.8	1.2	.763	1.070	1.075
1.8	1.3	.746	1.069	1.075
1.8	1.4	.731	1.067	1.072
1.8	1.5	.717	1.064	1.068
1.8	1.6	.705	1.059	1.062
1.8	1.7	.693	1.054	1.055
1.8	1.8	.683	1.049	1.048
1.8	1.9	.674	1.043	1.040
1.8	2.0	.665	1.037	1.032
1.9	1.0	.778	1.073	1.073
1.9	1.1	.758	1.079	1.081
1.9	1.2	.739	1.082	1.085
1.9	1.3	.723	1.082	1.085
1.9	1.4	.708	1.081	1.083
1.9	1.5	.695	1.079	1.079
1.9	1.6	.682	1.075	1.074
1.9	1.7	.671	1.070	1.067
1.9	1.8	.661	1.065	1.060
1.9	1.9	.652	1.060	1.053
2.0	2.0	.643	1.054	1.045
2.0	1.0	.756	1.083	1.083
2.0	1.1	.736	1.090	1.092
2.0	1.2	.717	1.095	1.096
2.0	1.3	.701	1.096	1.097
2.0	1.4	.687	1.096	1.095
2.0	1.5	.673	1.094	1.092
2.0	1.6	.661	1.091	1.087
2.0	1.7	.651	1.087	1.081
2.0	1.8	.641	1.083	1.074
2.0	1.9	.632	1.078	1.067
2.0	2.0	.624	1.072	1.060

A/B	B/C	MU(A)	MU(B)	MU(C)
1.0	1.0	1.000	1.000	1.000
1.0	1.1	.995	.995	1.012
1.0	1.2	.991	.991	1.023
1.0	1.3	.990	.990	1.033
1.0	1.4	.989	.989	1.041
1.0	1.5	.990	.990	1.048
1.0	1.6	.991	.991	1.055
1.0	1.7	.993	.993	1.061
1.0	1.8	.995	.995	1.067
1.0	1.9	.998	.998	1.072
1.0	2.0	1.000	1.000	1.076
1.1	1.0	.987	1.007	1.007
1.1	1.1	.981	1.004	1.019
1.1	1.2	.978	1.003	1.030
1.1	1.3	.976	1.003	1.039
1.1	1.4	.975	1.005	1.047
1.1	1.5	.975	1.007	1.055
1.1	1.6	.976	1.009	1.061
1.1	1.7	.978	1.012	1.067
1.1	1.8	.980	1.015	1.072
1.1	1.9	.982	1.018	1.077
1.1	2.0	.984	1.022	1.081
1.2	1.0	.975	1.016	1.016
1.2	1.1	.969	1.015	1.028
1.2	1.2	.965	1.015	1.038
1.2	1.3	.963	1.017	1.047
1.2	1.4	.962	1.020	1.055
1.2	1.5	.962	1.023	1.062
1.2	1.6	.962	1.027	1.068
1.2	1.7	.963	1.030	1.074
1.2	1.8	.965	1.034	1.079
1.2	1.9	.967	1.038	1.084
1.2	2.0	.969	1.042	1.088
1.3	1.0	.963	1.025	1.025
1.3	1.1	.952	1.028	1.047
1.3	1.2	.950	1.031	1.056
1.3	1.3	.949	1.035	1.063
1.3	1.4	.948	1.039	1.070
1.3	1.5	.949	1.044	1.077
1.3	1.6	.949	1.048	1.082
1.3	1.7	.950	1.053	1.087
1.3	1.8	.951	1.057	1.092
1.3	1.9	.953	1.062	1.096
1.3	2.0	.955	1.035	1.035
1.4	1.0	.951	1.037	1.046
1.4	1.1	.945	1.041	1.056
1.4	1.2	.940	1.045	1.065
1.4	1.3	.938	1.050	1.073
1.4	1.4	.936	1.055	1.080
1.4	1.5	.936	1.060	1.086
1.4	1.6	.937	1.066	1.091
1.4	1.7	.938	1.071	1.096
1.4	1.8	.939	1.076	1.101
1.4	1.9	.941	1.081	1.105
1.4	2.0	.940	1.045	1.045
1.5	1.0	.940	1.049	1.056
1.5	1.1	.934	1.054	1.066
1.5	1.2	.929	1.059	1.075
1.5	1.3	.926	1.059	1.082
1.5	1.4	.925	1.065	1.095
1.5	1.5	.924	1.071	1.101
1.5	1.6	.924	1.082	1.105
1.5	1.7	.924	1.088	1.110
1.5	1.8	.925	1.094	1.114
1.5	1.9	.927	1.099	1.114
1.5	2.0	.928	1.056	1.056
1.6	1.0	.930	1.061	1.067
1.6	1.1	.923	1.067	1.076
1.6	1.2	.918	1.073	1.085
1.6	1.3	.915	1.080	1.092
1.6	1.4	.913	1.086	1.099
1.6	1.5	.912	1.092	1.105
1.6	1.6	.912	1.099	1.110
1.6	1.7	.913	1.105	1.115
1.6	1.8	.913	1.111	1.119
1.6	1.9	.915	1.116	1.123
1.6	2.0	.916	1.066	1.066
1.7	1.0	.920	1.073	1.077
1.7	1.1	.913	1.080	1.087
1.7	1.2	.908	1.087	1.095
1.7	1.3	.905	1.094	1.103
1.7	1.4	.903	1.094	1.109
1.7	1.5	.901	1.101	1.115
1.7	1.6	.901	1.108	

1.7	1.7	•901	1.114	1.120
1.7	1.8	•902	1.121	1.125
1.7	1.9	•903	1.127	1.129
1.7	2.0	•904	1.133	1.133
1.8	1.0	•910	1.077	1.077
1.8	1.1	•903	1.084	1.088
1.8	1.2	•898	1.092	1.097
1.8	1.3	•894	1.100	1.105
1.8	1.4	•892	1.108	1.113
1.8	1.5	•891	1.115	1.119
1.8	1.6	•890	1.122	1.125
1.8	1.7	•891	1.129	1.130
1.8	1.8	•891	1.136	1.135
1.8	1.9	•892	1.142	1.139
1.8	2.0	•893	1.149	1.143
1.9	1.0	•901	1.087	1.087
1.9	1.1	•893	1.096	1.098
1.9	1.2	•888	1.104	1.108
1.9	1.3	•885	1.113	1.116
1.9	1.4	•882	1.121	1.123
1.9	1.5	•881	1.129	1.129
1.9	1.6	•880	1.137	1.135
1.9	1.7	•880	1.144	1.140
1.9	1.8	•881	1.151	1.145
1.9	1.9	•881	1.157	1.149
1.9	2.0	•882	1.164	1.153
2.0	1.0	•892	1.098	1.098
2.0	1.1	•884	1.107	1.109
2.0	1.2	•879	1.116	1.118
2.0	1.3	•875	1.125	1.126
2.0	1.4	•873	1.134	1.133
2.0	1.5	•871	1.142	1.140
2.0	1.6	•870	1.150	1.145
2.0	1.7	•870	1.158	1.150
2.0	1.8	•870	1.165	1.155
2.0	1.9	•871	1.172	1.159
2.0	2.0	•872	1.178	1.163

A/B	B/C	THETA+	THETA-	TAU/TAU0	PSI
1.0	1.0	.167	.167	1.000	1.000
1.0	1.1	.169	.163	1.004	.998
1.0	1.2	.170	.159	1.014	.997
1.0	1.3	.169	.155	1.029	.995
1.0	1.4	.167	.151	1.047	.992
1.0	1.5	.165	.147	1.069	.989
1.0	1.6	.162	.143	1.094	.986
1.0	1.7	.158	.139	1.121	.983
1.0	1.8	.155	.135	1.150	.980
1.0	1.9	.151	.132	1.180	.977
1.0	2.0	.147	.128	1.211	1.000
1.1	1.0	.170	.163	1.004	.999
1.1	1.1	.170	.159	1.011	.997
1.1	1.2	.170	.155	1.024	.995
1.1	1.3	.169	.151	1.042	.993
1.1	1.4	.166	.147	1.064	.990
1.1	1.5	.163	.143	1.089	.987
1.1	1.6	.160	.139	1.117	.984
1.1	1.7	.156	.134	1.147	.981
1.1	1.8	.149	.127	1.178	.978
1.1	1.9	.145	.123	1.211	.975
1.1	2.0	.172	.158	1.013	.999
1.2	1.0	.172	.154	1.023	.998
1.2	1.1	.172	.150	1.040	.996
1.2	1.2	.171	.145	1.061	.994
1.2	1.3	.169	.141	1.085	.991
1.2	1.4	.163	.137	1.113	.988
1.2	1.5	.159	.132	1.143	.985
1.2	1.6	.155	.128	1.175	.982
1.2	1.7	.152	.124	1.209	.979
1.2	1.8	.148	.120	1.244	.976
1.2	1.9	.144	.117	1.281	.972
1.3	1.0	.173	.152	1.026	.998
1.3	1.1	.173	.148	1.040	.996
1.3	1.2	.172	.143	1.059	.994
1.3	1.3	.169	.139	1.082	.992
1.3	1.4	.166	.134	1.109	.989
1.3	1.5	.163	.130	1.139	.986
1.3	1.6	.159	.125	1.172	.983
1.3	1.7	.155	.121	1.206	.980
1.3	1.8	.151	.117	1.242	.977
1.3	1.9	.147	.114	1.279	.974
1.3	2.0	.143	.110	1.318	.971
1.4	1.0	.174	.146	1.043	.996
1.4	1.1	.174	.141	1.059	.995
1.4	1.2	.172	.137	1.080	.993
1.4	1.3	.170	.132	1.106	.991
1.4	1.4	.166	.127	1.135	.988
1.4	1.5	.163	.123	1.167	.985
1.4	1.6	.159	.119	1.201	.982
1.4	1.7	.155	.114	1.238	.979
1.4	1.8	.151	.111	1.276	.976
1.4	1.9	.147	.107	1.315	.972
1.4	2.0	.143	.103	1.356	.969
1.5	1.0	.174	.140	1.061	.995
1.5	1.1	.174	.135	1.079	.994
1.5	1.2	.172	.130	1.103	.992
1.5	1.3	.170	.125	1.130	.989
1.5	1.4	.166	.121	1.161	.987
1.5	1.5	.163	.116	1.195	.984
1.5	1.6	.159	.112	1.232	.981
1.5	1.7	.155	.108	1.270	.978
1.5	1.8	.150	.104	1.310	.975
1.5	1.9	.146	.101	1.351	.972
1.5	2.0	.142	.097	1.393	.969
1.5	1.0	.175	.134	1.081	.994
1.6	1.1	.174	.129	1.101	.993
1.6	1.2	.172	.124	1.126	.991
1.6	1.3	.170	.119	1.156	.988
1.6	1.4	.166	.114	1.189	.986
1.6	1.5	.162	.110	1.224	.983
1.6	1.6	.158	.106	1.262	.980
1.6	1.7	.154	.102	1.302	.977
1.6	1.8	.150	.098	1.344	.974
1.6	1.9	.146	.095	1.386	.971
1.6	2.0	.142	.091	1.430	.969
1.7	1.0	.175	.127	1.102	.993
1.7	1.1	.174	.122	1.124	.992
1.7	1.2	.172	.117	1.151	.990
1.7	1.3	.169	.113	1.182	.988
1.7	1.4	.166	.108	1.216	.985
1.7	1.5	.162	.104	1.253	.983
1.7	1.6	.158	.100	1.293	.980

1.7	1.7	.154	.096	1.334	.977
1.7	1.8	.150	.092	1.377	.974
1.7	1.9	.145	.089	1.422	.972
1.7	2.0	.141	.086	1.467	.969
1.8	1.0	.175	.122	1.124	.992
1.8	1.1	.174	.117	1.147	.991
1.8	1.2	.172	.112	1.175	.990
1.8	1.3	.169	.107	1.207	.988
1.8	1.4	.166	.102	1.243	.985
1.8	1.5	.162	.098	1.282	.983
1.8	1.6	.158	.094	1.323	.980
1.8	1.7	.154	.091	1.366	.978
1.8	1.8	.149	.087	1.410	.975
1.8	1.9	.145	.084	1.456	.972
1.8	2.0	.141	.081	1.503	.970
1.9	1.0	.175	.116	1.146	.992
1.9	1.1	.174	.111	1.170	.991
1.9	1.2	.172	.106	1.199	.989
1.9	1.3	.169	.101	1.233	.988
1.9	1.4	.165	.097	1.270	.986
1.9	1.5	.162	.093	1.310	.983
1.9	1.6	.157	.089	1.352	.981
1.9	1.7	.153	.086	1.396	.978
1.9	1.8	.149	.082	1.442	.976
1.9	1.9	.145	.079	1.489	.973
1.9	2.0	.141	.076	1.538	.971
2.0	1.0	.175	.111	1.168	.991
2.0	1.1	.174	.106	1.193	.991
2.0	1.2	.172	.101	1.224	.990
2.0	1.3	.169	.096	1.258	.988
2.0	1.4	.165	.092	1.296	.986
2.0	1.5	.161	.088	1.337	.984
2.0	1.6	.157	.084	1.381	.982
2.0	1.7	.153	.081	1.426	.979
2.0	1.8	.149	.078	1.473	.977
2.0	1.9	.144	.075	1.522	.975
2.0	2.0	.140	.072	1.571	.972

A/8	B/C	DELTA+	DELTA-
1.0	1.0	2.500	2.500
1.0	1.1	2.541	2.454
1.0	1.2	2.568	2.413
1.0	1.3	2.582	2.377
1.0	1.4	2.588	2.344
1.0	1.5	2.586	2.314
1.0	1.6	2.579	2.286
1.0	1.7	2.568	2.259
1.0	1.8	2.555	2.235
1.0	1.9	2.539	2.212
1.0	2.0	2.522	2.190
1.1	1.0	2.549	2.446
1.1	1.1	2.577	2.410
1.1	1.2	2.596	2.372
1.1	1.3	2.605	2.337
1.1	1.4	2.606	2.305
1.1	1.5	2.601	2.274
1.1	1.6	2.592	2.246
1.1	1.7	2.579	2.220
1.1	1.8	2.564	2.195
1.1	1.9	2.547	2.172
1.1	2.0	2.529	2.151
1.2	1.0	2.599	2.387
1.2	1.1	2.624	2.350
1.2	1.2	2.641	2.313
1.2	1.3	2.648	2.277
1.2	1.4	2.642	2.245
1.2	1.5	2.632	2.214
1.2	1.6	2.619	2.185
1.2	1.7	2.604	2.159
1.2	1.8	2.587	2.134
1.2	1.9	2.570	2.111
1.2	2.0	2.648	2.089
1.3	1.0	2.675	2.326
1.3	1.1	2.692	2.286
1.3	1.2	2.700	2.248
1.3	1.3	2.700	2.212
1.3	1.4	2.695	2.178
1.3	1.5	2.686	2.147
1.3	1.6	2.674	2.118
1.3	1.7	2.660	2.091
1.3	1.8	2.644	2.066
1.3	1.9	2.627	2.043
1.3	2.0	2.699	2.021
1.4	1.0	2.729	2.264
1.4	1.1	2.748	2.222
1.4	1.2	2.757	2.183
1.4	1.3	2.759	2.146
1.4	1.4	2.756	2.112
1.4	1.5	2.748	2.081
1.4	1.6	2.737	2.051
1.4	1.7	2.724	2.024
1.4	1.8	2.710	1.999
1.4	1.9	2.694	1.976
1.4	2.0	2.752	1.954
1.5	1.0	2.785	2.203
1.5	1.1	2.807	2.160
1.5	1.2	2.818	2.119
1.5	1.3	2.823	2.082
1.5	1.4	2.821	2.048
1.5	1.5	2.815	2.016
1.5	1.6	2.806	1.987
1.5	1.7	2.795	1.961
1.5	1.8	2.781	1.936
1.5	1.9	2.767	1.913
1.5	2.0	2.806	1.892
1.6	1.0	2.844	2.144
1.6	1.1	2.868	2.100
1.6	1.2	2.883	2.059
1.6	1.3	2.890	2.021
1.6	1.4	2.891	1.987
1.6	1.5	2.887	1.956
1.6	1.6	2.880	1.927
1.6	1.7	2.870	1.901
1.6	1.8	2.858	1.877
1.6	1.9	2.845	1.854
1.6	2.0	2.863	1.834
1.7	1.0	2.905	1.887
1.7	1.1	2.933	2.042
1.7	1.2	2.951	2.001
1.7	1.3	2.961	1.964
1.7	1.4	2.965	1.930
1.7	1.5	2.965	1.899
1.7	1.6	2.963	1.871

1.7	1.7	2.958	1.845
1.7	1.8	2.949	1.822
1.7	1.9	2.939	1.800
1.7	2.0	2.927	1.780
1.8	1.0	2.922	2.033
1.8	1.1	2.968	1.987
1.8	1.2	3.001	1.946
1.8	1.3	3.023	1.910
1.8	1.4	3.036	1.876
1.8	1.5	3.042	1.846
1.8	1.6	3.042	1.819
1.8	1.7	3.039	1.794
1.8	1.8	3.033	1.771
1.8	1.9	3.024	1.750
1.8	2.0	3.014	1.730
1.9	1.0	2.983	1.981
1.9	1.1	3.035	1.936
1.9	1.2	3.071	1.895
1.9	1.3	3.097	1.859
1.9	1.4	3.113	1.826
1.9	1.5	3.122	1.797
1.9	1.6	3.125	1.770
1.9	1.7	3.124	1.746
1.9	1.8	3.120	1.724
1.9	1.9	3.113	1.703
1.9	2.0	3.104	1.685
2.0	1.0	3.047	1.932
2.0	1.1	3.103	1.887
2.0	1.2	3.145	1.847
2.0	1.3	3.174	1.812
2.0	1.4	3.194	1.780
2.0	1.5	3.206	1.751
2.0	1.6	3.212	1.725
2.0	1.7	3.213	1.702
2.0	1.8	3.210	1.680
2.0	1.9	3.205	1.661
2.0	2.0	3.198	1.643

A/B	B/C	GAMMA+	GAMMA-
1.0	1.0	1.0000	1.000
1.0	1.1	1.0016	.981
1.0	1.2	1.0026	.965
1.0	1.3	1.0031	.949
1.0	1.4	1.0032	.935
1.0	1.5	1.0031	.922
1.0	1.6	1.0027	.910
1.0	1.7	1.0021	.898
1.0	1.8	1.0015	.888
1.0	1.9	1.0008	.878
1.0	2.0	1.0000	.868
1.1	1.0	1.0020	.978
1.1	1.1	1.0030	.963
1.1	1.2	1.0037	.947
1.1	1.3	1.0039	.932
1.1	1.4	1.0039	.918
1.1	1.5	1.0035	.905
1.1	1.6	1.0030	.893
1.1	1.7	1.0024	.881
1.1	1.8	1.0017	.871
1.1	1.9	1.0009	.861
1.1	2.0	1.0001	.851
1.2	1.0	1.0038	.954
1.2	1.1	1.0048	.938
1.2	1.2	1.0053	.922
1.2	1.3	1.0055	.907
1.2	1.4	1.0050	.893
1.2	1.5	1.0044	.880
1.2	1.6	1.0038	.867
1.2	1.7	1.0030	.855
1.2	1.8	1.0023	.844
1.2	1.9	1.0015	.834
1.2	2.0	1.0015	.825
1.3	1.0	1.0057	.928
1.3	1.1	1.0066	.911
1.3	1.2	1.0072	.895
1.3	1.3	1.0073	.879
1.3	1.4	1.0072	.865
1.3	1.5	1.0068	.851
1.3	1.6	1.0063	.838
1.3	1.7	1.0057	.826
1.3	1.8	1.0049	.815
1.3	1.9	1.0042	.805
1.3	2.0	1.0034	.795
1.4	1.0	1.0075	.902
1.4	1.1	1.0085	.884
1.4	1.2	1.0091	.867
1.4	1.3	1.0093	.851
1.4	1.4	1.0092	.836
1.4	1.5	1.0089	.822
1.4	1.6	1.0084	.809
1.4	1.7	1.0078	.797
1.4	1.8	1.0071	.786
1.4	1.9	1.0064	.776
1.4	2.0	1.0056	.766
1.5	1.0	1.0094	.876
1.5	1.1	1.0105	.857
1.5	1.2	1.0111	.839
1.5	1.3	1.0114	.823
1.5	1.4	1.0113	.808
1.5	1.5	1.0111	.794
1.5	1.6	1.0106	.781
1.5	1.7	1.0101	.769
1.5	1.8	1.0094	.758
1.5	1.9	1.0087	.748
1.5	2.0	1.0080	.738
1.6	1.0	1.0113	.850
1.6	1.1	1.0125	.831
1.6	1.2	1.0132	.812
1.6	1.3	1.0135	.796
1.6	1.4	1.0136	.781
1.6	1.5	1.0133	.767
1.6	1.6	1.0130	.754
1.6	1.7	1.0125	.742
1.6	1.8	1.0119	.731
1.6	1.9	1.0112	.721
1.6	2.0	1.0105	.712
1.7	1.0	1.0132	.825
1.7	1.1	1.0145	.805
1.7	1.2	1.0154	.787
1.7	1.3	1.0158	.770
1.7	1.4	1.0159	.755
1.7	1.5	1.0157	.741
1.7	1.6	1.0154	.729

1.7	1.7	1.149	.717
1.7	1.8	1.144	.706
1.7	1.9	1.138	.697
1.7	2.0	1.131	.688
1.8	1.0	1.151	.801
1.8	1.1	1.166	.781
1.8	1.2	1.176	.762
1.8	1.3	1.181	.746
1.8	1.4	1.182	.731
1.8	1.5	1.182	.717
1.8	1.6	1.179	.705
1.8	1.7	1.175	.693
1.8	1.8	1.170	.683
1.8	1.9	1.164	.674
1.8	2.0	1.158	.665
1.9	1.0	1.172	.778
1.9	1.1	1.188	.758
1.9	1.2	1.198	.739
1.9	1.3	1.204	.723
1.9	1.4	1.207	.708
1.9	1.5	1.207	.695
1.9	1.6	1.205	.682
1.9	1.7	1.201	.671
1.9	1.8	1.197	.661
1.9	1.9	1.191	.652
2.0	2.0	1.185	.643
2.0	1.0	1.192	.756
2.0	1.1	1.210	.736
2.0	1.2	1.221	.717
2.0	1.3	1.229	.701
2.0	1.4	1.232	.687
2.0	1.5	1.233	.673
2.0	1.6	1.231	.661
2.0	1.7	1.229	.651
2.0	1.8	1.224	.641
2.0	1.9	1.219	.632
2.0	2.0	1.214	.624

### Program 3

```

***** THIS PROGRAM PRODUCES A CONTOUR MAP OF THE VISCOSITY
INCREMENT OVER THE AXIAL RANGE A/B, B/C 1.0 TO 3.0, IN
STEPS OF 0.5 OF THE FUNCTION FROM NU=2.5 TO NU=7.0 *****
***** PROGRAM MAIN(INPUT,OUTPUT,TAPE2=INPUT,TAPE3=OUTPUT)
COMMON/PARAM/A,C,NN
EXTERNAL FUN
DIMENSION ALPHA(10,21,21),NU(21,21),H(10)
REAL NU
NN=0
COMPUTE THE ELLIPTIC INTEGRALS
D045 K=1,10
A=0.9
NN=NN+1
D040 I=1,21
A=A+0.1
C=1.0/0.9
D030 N=1,21
C=C/(1.0+0.1*C)
SET LIMITS FOR NUMERICAL INTEGRATION (THESE LIMITS
BELOW HAVE BEEN PREVIOUSLY TESTED FOR CONVERGENCE)
AA=0.0
BB=1000000
IF(NN.EQ.10)BB=500000000
MAXDIV=50
EPS=1.0E-08
ACC=0.0
IFAIL=0
CALL U.K. "NAG" LIBRARY ROUTINE FOR NUMERICAL EVALUATION
OF THE INTEGRALS "ALPHA" GIVEN IN THE SUBROUTINE BELOW
CALL D01AGF(AA,BB,FUN,MAXDIV,EPS,ACC,ANS,ERROR,NOFUN,IFAIL)
ALPHA(NN,I,N)=ANS
30 CONTINUE
40 CONTINUE
45 CONTINUE
B=1.0
A=0.9
D080 J=1,21
A=A+0.1
C=1.0/0.9
D070 N=1,21
C=C/(1.0+0.1*C)
NOW COMPUTE THE FUNCTION VALUES USING THE STORED INTEGRAL VALUES
NU(J,N)=(1.0/(A*B*C))*((4.0/15.0)*((ALPHA(7,J,N)+ALPHA(8,J,N)
+ +ALPHA(9,J,N))/(ALPHA(8,J,N)*ALPHA(9,J,N)+ALPHA(9,J,N)*ALPHA
+ +(7,J,N)+ALPHA(7,J,N)*ALPHA(8,J,N)))+(1.0/5.0)*(((ALPHA(2,J,N)
+ +ALPHA(3,J,N))/(ALPHA(4,J,N)*(B*B*ALPHA(2,J,N)+C*C*ALPHA(3,J,N)
+ ))+((ALPHA(3,J,N)+ALPHA(1,J,N))/(ALPHA(5,J,N)*(C*C*ALPHA(3,J,N)
+ +A*A*ALPHA(1,J,N))))+((ALPHA(1,J,N)+ALPHA(2,J,N))/(ALPHA(6,J,N)
+ +(A*A*ALPHA(1,J,N)+B*B*ALPHA(2,J,N)))))))
70 CONTINUE
80 CONTINUE
CALL CONTOUR PLOTTING ROUTINE
CALL PAPER(1)
H(1)=2.5
H(2)=3.0
H(3)=3.5
H(4)=4.0
H(5)=4.5
H(6)=5.0
H(7)=5.5
H(8)=6.0
H(9)=6.5
H(10)=7.0
CALL MAP(1.0,3.0,1.0,3.0)
CALL SCALES
CALL BORDER
CALL CONTRL(NU,1,21,21,1,21,21,H,1,10)
CALL GREND
STOP
END

```

ccc

```

REAL FUNCTION FUN(X)
COMMON/PARAM/A,C,NN
B=1.0
GOTO(10,20,30,40,50,60,70,80,90,100),NN
10 FUN=1/((A*A+X)**1.5*(B*B+X)**0.5*(C*C+X)**0.5)
RETURN
20 FUN=1/((A*A+X)**0.5*(B*B+X)**1.5*(C*C+X)**0.5)
RETURN
30 FUN=1/((A*A+X)**0.5*(B*B+X)**0.5*(C*C+X)**1.5)
RETURN
40 FUN=1/((A*A+X)**0.5*(B*B+X)**1.5*(C*C+X)**1.5)
RETURN
50 FUN=1/((A*A+X)**1.5*(B*B+X)**0.5*(C*C+X)**1.5)
RETURN
60 FUN=1/((A*A+X)**1.5*(B*B+X)**1.5*(C*C+X)**0.5)
RETURN
70 FUN=X/((A*A+X)**0.5*(B*B+X)**1.5*(C*C+X)**1.5)
RETURN
80 FUN=X/((A*A+X)**1.5*(B*B+X)**0.5*(C*C+X)**1.5)
RETURN
90 FUN=X/((A*A+X)**1.5*(B*B+X)**1.5*(C*C+X)**0.5)
RETURN
100 FUN=1.0/(((A*A+X)*(B*B+X)*(C*C+X))**0.5)
RETURN
END

```

Program 4

```
*****
THIS PROGRAM GIVES PLOTS OF THE LINE SOLUTIONS OF THE
VARIOUS TRIAXIAL SHAPE FUNCTIONS ( AS TABULATED IN THE
PREVIOUS PROGRAM) FOR AXIAL RATIOS A/B = B/C = 1.5, IN
ORDER TO DETERMINE THE BEST COMBINATION FOR PRODUCING
A UNIQUE SOLUTION.
*****
```

```
PROGRAM MAIN(INPUT,OUTPUT,TAPE2=INPUT,TAPE3=OUTPUT)
COMMON/PARAM/A,C,NN
EXTERNAL FUN
DIMENSION ALPHA(10,21,21),NU(21,21),F(21,21),R(21,21),H(1)
+ ,BETA(21,21),CA(21,21),CB(21,21),CC(21,21),M(21,21),O(21,21)
+ ,P(21,21),TPLS(21,21),TMNS(21,21),RHOA(21,21),RHOB(21,21)
+ ,RHOC(21,21),TAU(21,21),PSI(21,21),DELA(21,21),DELB(21,21)
+ ,DELC(21,21),GAMMAA(21,21),GAMMAB(21,21),GAMMAC(21,21),MUA(21,21)
+ ,MUB(21,21),MUC(21,21),DPLS(21,21),DMNS(21,21),GPLS(21,21)
+ ,GMNS(21,21),V(21,21)
+ ,X1(21,21),X2(21,21),X3(21,21),X4(21,21),X5(21,21)
+ ,T1(21,21),T2(21,21),T3(21,21),T4(21,21),T5(21,21)
REAL NU,M,O,P,MUA,MUB,MUC,PSI
C COMPUTE THE ELLIPTIC INTEGRALS
NN=0
DO45 K=1,10
A=0.95
NN=NN+1
DO40 I=1,21
A=A+0.05
C=1.0/0.95
DO30 N=1,21
C=C/(1.0+0.05*C)
C SET LIMITS FOR NUMERICAL INTEGRATION (THESE LIMITS
BELOW HAVE BEEN PREVIOUSLY TESTED FOR CONVERGENCE)
AA=0.0
BB=1000000
IF(NN.EQ.10) BB=500000000
MAXDIV=50
EPS=1.0E-08
ACC=0.0
IFAIL=0
CALL U.K. "NAG" LIBRARY ROUTINE FOR NUMERICAL EVALUATION
OF THE INTEGRALS "ALPHA" GIVEN IN THE SUBROUTINE BELOW
CALL D01AGF(AA,BB,FUN,MAXDIV,EPS,ACC,ANS,ERROR,NOFUN,IFAIL)
ALPHA(NN,I,N)=ANS
30 CONTINUE
40 CONTINUE
45 CONTINUE
B=1.0
A=0.95
DO80 J=1,21
A=A+0.05
C=1.0/0.95
DO70 N=1,21
C=C/(1.0+0.05*C)
C NOW COMPUTE THE FUNCTION VALUES USING THE STORED INTEGRAL VALUES
NU(J,N)=(1.0/(A*B*C))*((4.0/15.0)*((ALPHA(7,J,N)+ALPHA(8,J,N)
+ +ALPHA(9,J,N))/(ALPHA(8,J,N)*ALPHA(9,J,N)+ALPHA(9,J,N)*ALPHA
+ (7,J,N)+ALPHA(7,J,N)*ALPHA(8,J,N)))+(1.0/5.0)*(((ALPHA(2,J,N)
+ +ALPHA(3,J,N))/(ALPHA(4,J,N)*(B*B*ALPHA(2,J,N)+C*C*ALPHA(3,J,N)
+ ))+((ALPHA(3,J,N)+ALPHA(1,J,N))/(ALPHA(5,J,N)*(C*C*ALPHA(3,J,N)
+ +A*A*ALPHA(1,J,N))))+((ALPHA(1,J,N)+ALPHA(2,J,N))/(ALPHA(6,J,N)
+ +(A*A*ALPHA(1,J,N)+B*B*ALPHA(2,J,N))))))
F(J,N)=2.0/(((A*B*C)**(1.0/3.0))*ALPHA(10,J,N))
R(J,N)=2.0*(1.0+(F(J,N)**3.0))/NU(J,N)
BETA(J,N)=(1.0/1000000.0)*((6.0249**1.0/3.0)*(1.0**23.0/3.0
+ ))/((16200.0*3.141592654*3.141592654)**(1.0/3.0))*(NU(J,N)
+ **(1.0/3.0))/F(J,N)
M(J,N)=(B*B+C*C)/(B*B*ALPHA(2,J,N)+C*C*ALPHA(3,J,N))
O(J,N)=(C*C+A*A)/(C*C*ALPHA(3,J,N)+A*A*ALPHA(1,J,N))
P(J,N)=(A*A+B*B)/(A*A*ALPHA(1,J,N)+B*B*ALPHA(2,J,N))
TPLS(J,N)=((A*B*C)/(12.0))*((((1.0/M(J,N))+(1.0/O(J,N))+(1.0/P(J,
+ N)))+((1.0/M(J,N)**2.0)+(1.0/O(J,N)**2.0)+(1.0/P(J,N)**2.0))-
+ ((1.0/(M(J,N)*O(J,N)))+(1.0/(O(J,N)*P(J,N)))+(1.0/(P(J,N)*M(J,
+ N)))))**0.5))
TMNS(J,N)=((A*B*C)/(12.0))*((((1.0/M(J,N))+(1.0/O(J,N))+(1.0/P(J,
+ N)))-((1.0/M(J,N)**2.0)+(1.0/O(J,N)**2.0)+(1.0/P(J,N)**2.0))-
+ ((1.0/(M(J,N)*O(J,N)))+(1.0/(O(J,N)*P(J,N)))+(1.0/(P(J,N)*M(J,
+ N)))))**0.5))
CA(J,N)=(2.0/(3.0*A*B*C))*M(J,N)
CB(J,N)=(2.0/(3.0*A*B*C))*O(J,N)
```

```

CC(J,N)=(2.0/(3.0*A*B*C))*P(J,N)
RHOA(J,N)=2.0/((1.0/CB(J,N))+(1.0/CC(J,N)))
RHOB(J,N)=2.0/((1.0/CA(J,N))+(1.0/CC(J,N)))
RHOC(J,N)=2.0/((1.0/CA(J,N))+(1.0/CB(J,N)))
DELA(J,N)=NU(J,N)/CA(J,N)
DELB(J,N)=NU(J,N)/CB(J,N)
DELC(J,N)=NU(J,N)/CC(J,N)
TAU(J,N)=3.0/((1.0/CA(J,N))+(1.0/CB(J,N))+(1.0/CC(J,N)))
PSI(J,N)=F(J,N)*(1.0/TAU(J,N))**(1.0/3.0)
V(J,N)=NU(J,N)/TAU(J,N)
X1(J,N)=0.5*((1.0/RHOB(J,N))+(1.0/RHOC(J,N))-(1.0/RHOA(J,N)))
X2(J,N)=0.5*((1.0/RHOC(J,N))+(1.0/RHOA(J,N))-(1.0/RHOB(J,N)))
X3(J,N)=0.5*((1.0/RHOA(J,N))+(1.0/RHOB(J,N))-(1.0/RHOC(J,N)))
X4(J,N)=(X1(J,N)+X2(J,N)+X3(J,N))/3.0
X5(J,N)=((X1(J,N)**2.0)+(X2(J,N)**2.0)+(X3(J,N)**2.0)-(X1(J,N)*X2
+(J,N))-(X2(J,N)*X3(J,N))-(X3(J,N)*X1(J,N)))**0.5
T1(J,N)=1.0/(X4(J,N)+X1(J,N))
T2(J,N)=1.0/(X4(J,N)+X2(J,N))
T3(J,N)=1.0/(X4(J,N)+X3(J,N))
T4(J,N)=3.0/((6.0*X4(J,N))-(2.0*X5(J,N)))
T5(J,N)=3.0/((6.0*X4(J,N))+(2.0*X5(J,N)))
GAMMAA(J,N)=(1.0/2.0)*(F(J,N)**3.0)*((1.0/CB(J,N))+(1.0/CC(J,N)))
GAMMAB(J,N)=(1.0/2.0)*(F(J,N)**3.0)*((1.0/CA(J,N))+(1.0/CC(J,N)))
GAMMAC(J,N)=(1.0/2.0)*(F(J,N)**3.0)*((1.0/CA(J,N))+(1.0/CB(J,N)))
MUA(J,N)=(CA(J,N)**(1.0/3.0))/F(J,N)
MUB(J,N)=(CB(J,N)**(1.0/3.0))/F(J,N)
MUC(J,N)=(CC(J,N)**(1.0/3.0))/F(J,N)
DPLS(J,N)=6.0*TPLS(J,N)*NU(J,N)
DMNS(J,N)=6.0*TMNS(J,N)*NU(J,N)
GPLS(J,N)=6.0*TPLS(J,N)*(F(J,N)**3.0)
GMNS(J,N)=6.0*TMNS(J,N)*(F(J,N)**3.0)

```

70 CONTINUE

80 CONTINUE

```

CALL PAPER(1)
CALL MAP(1.0,2.0,1.0,2.0)
CALL SCALSI(0.1,0.1)
CALL GPSTOP(21)
CALL BORDER
CALL CSPACE(0.0,0.0001,0.0,0.0001)

```

(I) PLOT OF VISCOSITY INCREMENT AND PERRIN TRANSLATIONAL  
FRICTIONAL FUNCTION

```

H(1)=2.892
CALL CONTRL(NU,1,21,21,1,21,21,H,1,1)
CALL REDOPEN
H(1)=1.044
CALL CONTRL(F,1,21,21,1,21,21,H,1,1)

```

(II) PLOT OF THE TRANSLATIONAL FUNCTIONS: THE VISCOSITY INCREMENT  
THE PERRIN FUNCTION, THE BETA FUNCTION AND THE R FUNCTION, ALL  
WITH +/-1% ASSUMED EXPERIMENTAL ERROR

```

CALL FRAME
CALL BLKPEN
CALL BORDER
CALL CSPACE(0.0,1.0,0.0,1.0)
CALL SCALSI(0.1,0.1)
CALL CSPACE(0.0,0.0001,0.0,0.0001)
H(1)=2.92092
CALL CONTRL(NU,1,21,21,1,21,21,H,1,1)
H(1)=2.86308
CALL CONTRL(NU,1,21,21,1,21,21,H,1,1)
H(1)=2.14423
CALL REDOPEN
CALL CONTRL(BETA,1,21,21,1,21,21,H,1,1)
H(1)=2.10177
CALL CONTRL(BETA,1,21,21,1,21,21,H,1,1)
H(1)=1.05444
CALL GRNPEN
CALL CONTRL(F,1,21,21,1,21,21,H,1,1)
H(1)=1.03356
CALL CONTRL(F,1,21,21,1,21,21,H,1,1)
H(1)=1.49379
CALL BROKEN(4,8,8,8)
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
H(1)=1.46421
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)

```

(III) PLOT OF THE R FUNCTION AND ROTATIONAL RELAXATION  
TIME RATIOS

```

CALL FRAME
CALL FULL
CALL BLKPEN
CALL BORDER
CALL CSPACE(0.0,1.0,0.0,1.0)
CALL SCALSI(0.1,0.1)
CALL CSPACE(0.0,0.0001,0.0,0.0001)
H(1)=1.479
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
H(1)=1.433
CALL CONTRL(RHOA,1,21,21,1,21,21,H,1,1)
H(1)=1.115
CALL REDPEN
CALL CONTRL(RHOB,1,21,21,1,21,21,H,1,1)
H(1)=1.093
CALL GRNPEN
CALL CONTRL(RHOC,1,21,21,1,21,21,H,1,1)

```

(IV) PLOT OF THE R FUNCTION WITH +/- 1% ASSUMED ERROR AND THE ROTATIONAL RELAXATION TIME RATIOS WITH +/- 2% ASSUMED ERROR

(IV) PLOT OF THE R FUNCTION, HARMONIC MEAN RELAXATION TIME  
RATIO (TH/T0) THE PSI & LAMBDA FUNCTIONS

```

CALL FRAME
CALL BLKPEN
CALL BORDER
CALL CSPACE(0.0,1.0,0.0,1.0)
CALL SCALSI(0.1,0.1)
CALL CSPACE(0.0,0.0001,0.0,0.0001)
H(1)=1.479
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
H(1)=1.195
CALL CONTRL(TAU,1,21,21,1,21,21,H,1,1)
H(1)=.98378
CALL REDPEN
CALL CONTRL(PSI,1,21,21,1,21,21,H,1,1)
H(1)=2.41886
CALL GRNPEN
CALL CONTRL(V,1,21,21,1,21,21,H,1,1)

```

(V) PLOT OF THE R FUNCTION (+/- 1%) , THE HARMONIC MEAN RELAXATION TIME RATIO (+/- 1%) AND THE PSI FUNCTION (+/- 2%) & THE LAMBDA FUNCTION (+/- 2%)

```
CALL FRAME
CALL BLKPEN
CALL BORDER
CALL CSPACE(0.0,1.0,0.0,1.0)
CALL SCALSI(0.1,0.1)
CALL CSPACE(0.0,0.0001,0.0,0.0001)
H(1)=1.49379
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
H(1)=1.46421
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
H(1)=1.20695
CALL CONTRL(TAU,1,21,21,1,21,21,H,1,1)
H(1)=1.18305
CALL CONTRL(TAU,1,21,21,1,21,21,H,1,1)
H(1)=1.0034556
CALL REDPEN
CALL CONTRL(PSI,1,21,21,1,21,21,H,1,1)
H(1)=0.9641044
CALL CONTRL(PSI,1,21,21,1,21,21,H,1,1)
CALL GRNPEN
H(1)=2.4672372
CALL CONTRL(V,1,21,21,1,21,21,H,1,1)
H(1)=2.3704828
CALL CONTRL(V,1,21,21,1,21,21,H,1,1)
```

(VI) PLOT OF R (+/-1%), DELTA1 (+/-1%), DELTA2 (+/-1%)  
AND DELTA3 (+/-1%)

```
CALL FRAME
CALL BLKPEN
CALL BORDER
CALL CSPACE(0.0,1.0,0.0,1.0)
CALL SCALSI(0.1,0.1)
CALL CSPACE(0.0,0.0001,0.0,0.0001)
H(1)=1.49379
```

```

CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
H(1)=1.46421
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
H(1)=3.2849
CALL CONTRL(DELA,1,21,21,1,21,21,H,1,1)
H(1)=3.1560802
CALL CONTRL(DELA,1,21,21,1,21,21,H,1,1)
H(1)=2.110
CALL REDPEN
CALL CONTRL(DELB,1,21,21,1,21,21,H,1,1)
H(1)=2.072
CALL CONTRL(DELB,1,21,21,1,21,21,H,1,1)
H(1)=2.006
CALL GRNPEN
CALL CONTRL(DELC,1,21,21,1,21,21,H,1,1)
H(1)=1.928
CALL CONTRL(DELC,1,21,21,1,21,21,H,1,1)

```

CCC (VII) PLOT OF THE R, GAMMAA, GAMMAB AND GAMMAC FUNCTIONS

```

CALL FRAME
CALL BLKPEN
CALL BORDER
CALL CSPACE(0.0,1.0,0.0,1.0)
CALL SCALSI(0.1,0.1)
CALL CSPACE(0.0,0.0001,0.0,0.0001)
H(1)=1.479
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
H(1)=0.795
CALL CONTRL(GAMMAA,1,21,21,1,21,21,H,1,1)
H(1)=1.022
CALL REDPEN
CALL CONTRL(GAMMAB,1,21,21,1,21,21,H,1,1)
H(1)=1.042
CALL GRNPEN
CALL CONTRL(GAMMAC,1,21,21,1,21,21,H,1,1)

```

CCCC (VIII) PLOT OF R (+/-1%), GAMMAA (+/-1%), GAMMAB (+/-1%)  
AND GAMMAC (+/-1%)

```

CALL FRAME
CALL BLKPEN
CALL BORDER
CALL CSPACE(0.0,1.0,0.0,1.0)
CALL SCALSI(0.1,0.1)
CALL CSPACE(0.0,0.0001,0.0,0.0001)
H(1)=1.49379
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
H(1)=1.46421
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
H(1)=.81498
CALL CONTRL(GAMMAA,1,21,21,1,21,21,H,1,1)
H(1)=.78302
CALL CONTRL(GAMMAA,1,21,21,1,21,21,H,1,1)
H(1)=1.04244
CALL REDPEN
CALL CONTRL(GAMMAB,1,21,21,1,21,21,H,1,1)
H(1)=1.00156
CALL CONTRL(GAMMAB,1,21,21,1,21,21,H,1,1)
CALL GRNPEN
H(1)=1.06284
CALL CONTRL(GAMMAC,1,21,21,1,21,21,H,1,1)
H(1)=1.02116
CALL CONTRL(GAMMAC,1,21,21,1,21,21,H,1,1)

```

CCCC (IX) PLOT OF THE R ,MUA, MUB AND MUC FUNCTIONS

```

CALL FRAME
CALL BLKPEN
CALL BORDER
CALL CSPACE(0.0,1.0,0.0,1.0)
CALL SCALSI(0.1,0.1)
CALL CSPACE(0.0,0.0001,0.0,0.0001)
H(1)=1.479
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
H(1)=.924
CALL CONTRL(MUA,1,21,21,1,21,21,H,1,1)
CALL REDPEN
H(1)=1.071
CALL CONTRL(MUB,1,21,21,1,21,21,H,1,1)

```

CALL GRNPEN  
H(1)=1.089  
CALL CONTRL(MUC,1,21,21,1,21,21,H,1,1)

CCCCC

(X) PLOT OF R (+/-1%), MUA (+/-1%), MUB (+/-1%)  
AND MUC (+/-1%)

CALL FRAME  
CALL BLKPEN  
CALL BORDER  
CALL CSPACE(0.0,1.0,0.0,1.0)  
CALL SCALSI(0.1,0.1)  
CALL CSPACE(0.0,0.0001,0.0,0.0001)  
H(1)=1.49379  
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)  
H(1)=1.46421  
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)  
H(1)=.94248  
CALL CONTRL(MUA,1,21,21,1,21,21,H,1,1)  
H(1)=.90552  
CALL CONTRL(MUA,1,21,21,1,21,21,H,1,1)  
H(1)=1.90242  
CALL REDPEN  
CALL CONTRL(MUB,1,21,21,1,21,21,H,1,1)  
H(1)=1.04958  
CALL CONTRL(MUB,1,21,21,1,21,21,H,1,1)  
H(1)=1.11078  
CALL GRNPEN  
CALL CONTRL(MUC,1,21,21,1,21,21,H,1,1)  
H(1)=1.06722  
CALL CONTRL(MUC,1,21,21,1,21,21,H,1,1)

CCCCC

(XI) PLOT OF THE R, REDUCED THETA+ AND REDUCED  
THETA - FUNCTIONS

CALL FRAME  
CALL BLKPEN  
CALL BORDER  
CALL CSPACE(0.0,1.0,0.0,1.0)  
CALL SCALSI(0.1,0.1)  
CALL CSPACE(0.0,0.0001,0.0,0.0001)  
H(1)=1.479  
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)  
CALL REDPEN  
H(1)=.163  
CALL CONTRL(TPLS,1,21,21,1,21,21,H,1,1)  
CALL GRNPEN  
H(1)=.116  
CALL CONTRL(TMNS,1,21,21,1,21,21,H,1,1)

CCCC

(XII) PLOT OF THE R(+/-1%), REDUCED THETA+ (+/-1%)  
AND REDUCED THETA- (+/-1%) FUNCTIONS

CALL FRAME  
CALL BLKPEN  
CALL BORDER  
CALL CSPACE(0.0,1.0,0.0,1.0)  
CALL SCALSI(0.1,0.1)  
CALL CSPACE(0.0,0.0001,0.0,0.0001)  
H(1)=1.49379  
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)  
H(1)=1.46421  
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)  
CALL REDPEN  
H(1)=.16463  
CALL CONTRL(TPLS,1,21,21,1,21,21,H,1,1)  
H(1)=.16137  
CALL CONTRL(TPLS,1,21,21,1,21,21,H,1,1)  
CALL GRNPEN  
H(1)=.11716  
CALL CONTRL(TMNS,1,21,21,1,21,21,H,1,1)  
H(1)=.11484  
CALL CONTRL(TMNS,1,21,21,1,21,21,H,1,1)

CCCCC

(XIII) PLOT OF THE R, DELTA+ AND DELTA- FUNCTIONS

```

CALL FRAME
CALL BLKPEN
CALL BORDER
CALL CSPACE(0.0,1.0,0.0,1.0)
CALL SCALSI(0.1,0.1)
CALL CSPACE(0.0,0.0001,0.0,0.0001)
H(1)=1.479
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
CALL REDPEN
H(1)=2.821
CALL CONTRL(DPLS,1,21,21,1,21,21,H,1,1)
CALL GRNPEN
H(1)=2.016
CALL CONTRL(DMNS,1,21,21,1,21,21,H,1,1)

```

(XIV) PLOT OF R (+/-1%), DELTA+ (+/-2%) AND DELTA- (+/-2%)

```

CALL FRAME
CALL BLKPEN
CALL BORDER
CALL CSPACE(0.0,1.0,0.0,1.0)
CALL SCALSI(0.1,0.1)
CALL CSPACE(0.0,0.0001,0.0,0.0001)
H(1)=1.49379
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
H(1)=1.46421
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
CALL REDPEN
H(1)=2.87742
CALL CONTRL(DPLS,1,21,21,1,21,21,H,1,1)
H(1)=2.76458
CALL CONTRL(DPLS,1,21,21,1,21,21,H,1,1)
CALL GRNPEN
H(1)=2.05632
CALL CONTRL(DMNS,1,21,21,1,21,21,H,1,1)
H(1)=1.97568
CALL CONTRL(DMNS,1,21,21,1,21,21,H,1,1)

```

(XV) PLOT OF THE R, GAMMA+ AND GAMMA- FUNCTIONS

```

CALL FRAME
CALL BLKPEN
CALL BORDER
CALL CSPACE(0.0,1.0,0.0,1.0)
CALL SCALSI(0.1,0.1)
CALL CSPACE(0.0,0.0001,0.0,0.0001)
H(1)=1.479
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
CALL REDPEN
H(1)=1.111
CALL CONTRL(GPLS,1,21,21,1,21,21,H,1,1)
CALL GRNPEN
CALL CONTRL(GMNS,1,21,21,1,21,21,H,1,1)

```

(XVI) PLOT OF R(+/-1%), GAMMA+ (+/-2%) AND GAMMA- (+/-2%)

```

CALL FRAME
CALL BLKPEN
CALL BORDER
CALL CSPACE(0.0,1.0,0.0,1.0)
CALL SCALSI(0.1,0.1)
CALL CSPACE(0.0,0.0001,0.0,0.0001)
H(1)=1.49379
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
H(1)=1.46421
CALL CONTRL(R,1,21,21,1,21,21,H,1,1)
CALL REDPEN
H(1)=1.13322
CALL CONTRL(GPLS,1,21,21,1,21,21,H,1,1)
H(1)=1.08878
CALL CONTRL(GPLS,1,21,21,1,21,21,H,1,1)
CALL GRNPEN
H(1)=.80988
CALL CONTRL(GMNS,1,21,21,1,21,21,H,1,1)
H(1)=.77812

```

CALL CONTRL(GMNS,1,21,21,1,21,21,H,1,1)

(XVII) PLOT OF THE 5 FLUORESCENCE ANISOTROPY RELAXATION TIME RATIOS

```

CALL FRAME
CALL BLKPEN
CALL BORDER
CALL CSPACE(0.0,1.0,0.0,1.0)
CALL SCALSI(0.1,0.1)
CALL CSPACE(0.0,0.0001,0.0,0.0001)
H(1)=1.02536
CALL CONTRL(T1,1,21,21,1,21,21,H,1,1)
H(1)=1.28883
CALL REDPEN
CALL CONTRL(T2,1,21,21,1,21,21,H,1,1)
CALL GRNPEN
H(1)=1.31877
CALL CONTRL(T3,1,21,21,1,21,21,H,1,1)
CALL BROKEN(4,8,8,8)
H(1)=1.43405
CALL CONTRL(T4,1,21,21,1,21,21,H,1,1)
CALL BLKPEN
H(1)=1.02497
CALL CONTRL(T5,1,21,21,1,21,21,H,1,1)
STOP
END

```

```

REAL FUNCTION FUN(X)
COMMON/PARAM/A,C,NN
B=1.0
GOTO(10,20,30,40,50,60,70,80,90,100),NN
10 FUN=1/((A*A+X)**1.5*(B*B+X)**0.5*(C*C+X)**0.5)
RETURN
20 FUN=1/((A*A+X)**0.5*(B*B+X)**1.5*(C*C+X)**0.5)
RETURN
30 FUN=1/((A*A+X)**0.5*(B*B+X)**0.5*(C*C+X)**1.5)
RETURN
40 FUN=1/((A*A+X)**0.5*(B*B+X)**1.5*(C*C+X)**1.5)
RETURN
50 FUN=1/((A*A+X)**1.5*(B*B+X)**0.5*(C*C+X)**1.5)
RETURN
60 FUN=1/((A*A+X)**1.5*(B*B+X)**1.5*(C*C+X)**0.5)
RETURN
70 FUN=X/((A*A+X)**0.5*(B*B+X)**1.5*(C*C+X)**1.5)
RETURN
80 FUN=X/((A*A+X)**1.5*(B*B+X)**0.5*(C*C+X)**1.5)
RETURN
90 FUN=X/((A*A+X)**1.5*(B*B+X)**1.5*(C*C+X)**0.5)
RETURN
100 FUN=1.0/(((A*A+X)*(B*B+X)*(C*C+X))**0.5)
RETURN
END

```

Program 5

```

C NON-LINEAR LEAST SQUARES METHOD USING AN ALGORITHM OF GILL AND
C MURRAY (1976)
C GAMMA = BIREFRINGENCE (RADS), F = SUM OF SQUARES OF THE RESIDUALS
C DPLS = DELTA+, DMNS = DELTA-
C X(1) = CURRENT INITIAL GUESS FOR THETA+
C X(2) = " " " "
C X(3) = " " " " A'+-
C X(4) = " " " " A'-
C X1 = CURRENT ESTIMATE FOR THETA+
C X2 = " " " "
C X3 = " " " " A'+-
C X4 = " " " " A'-
C *****
C LINEAR TIME INCREASE, 100PTS.
C .001 DEGREES S.E.
C RANDOM NUMBER RUN 50
C *****
C PROTEIN 3
C *****
C PROGRAM MAIN(INPUT,OUTPUT,TAPE2=INPUT,TAPE3=OUTPUT)
C COMMON/PARAM/GAMMA(101),T(101),R(101)
C REAL BL(4),BU(4),X(4),F,W(54)
C REAL Q1,Q2,Q3,Q4,Q5
C INTEGER IBOUND,IFAIL,J,LIW,LW,N
C INTEGER IW(6)
C P=-1.0
C DO21 I=1,101
C P=P+1.0
C R(I)=P
C T(I)=R(I)*1.0E-09
C 21 CONTINUE
C WRITE(3,32)
C 32 FORMAT( " TIME(NS) GAMMA")
C G05BBF REINITIALIZES THE STREAM OF THE RANDOM NUMBERS
C CALL G05BBF
C CALCULATE THE UNPERTURBED DECAY CURVE
C D050 I=1,101
C GAMMA(I)=0.07*EXP(-T(I)*6.0*5.187243E06) +
C +0.05*EXP(-T(I)*6.0*4.167486E06)
C NOW PERTURB EACH OF THE 160 DATA POINTS USING A NORMAL PSEUDO-RANDOM
C NUMBER GENERATOR G05ADF
C GAMMA(I)=GAMMA(I)+((0.1*1.74555E-04)*G05ADF(Y))
C WRITE(3,33)R(I),GAMMA(I)
C 33 FORMAT( F10.5,F8.5)
C 50 CONTINUE
C N=4
C IBOUND=0
C Q1=1.0
C DO THE MINIMIZATION FOR 30 INITIAL GUESSES TO ATTEMPT TO AVOID
C SUBSIDIARY MINIMA
C D010 I=1,30
C CALL RECTANGULAR PSEUDO RANDOM NUMBER ROUTINE G05AAF
C Z=G05AAF(X)
C X(1)=4.0+2.0*Z
C X(2)=3.0+2.0*Z
C X(3)=6.0+2.0*Z
C X(4)=4.0+2.0*Z
C BL(1)=4.0
C BL(2)=3.0
C BL(3)=6.0
C BL(4)=4.0
C BU(1)=6.0
C BU(2)=5.0
C BU(3)=8.0
C BU(4)=6.0
C LIW=6
C LW=54
C IFAIL=1
C CALL E04JAF(N,IBOUND,BL,BU,X,F,IW,LIW,W,LW,IFAIL)
C IF(IFAIL.NE.0)WRITE(3,100)IFAIL
C IF(IFAIL.EQ.1)GOTO 20
C 100 FORMAT("ERROR EXIT TYPE",I3,"SEE ROUTINE MANUAL")
C WRITE(3,110)F
C WRITE(3,120)(X(J),J=1,4)
C 110 FORMAT( " FUNCTION VALUE ON EXIT IS",F15.12)

```

```

120 FORMAT( " THETA+",F10.7," THETA-",F10.7,"A ",F7.4,
+ " A-",F7.4)
IF(Q1.LE.F)GOTO 30
Q1=F
Q2=X(1)
Q3=X(2)
Q4=X(3)
Q5=X(4)
30 CONTINUE
WRITE(3,130)
130 FORMAT( " ")
WRITE(3,140)
140 FORMAT( " ")
10 CONTINUE
DPLS=0.50996303*Q2
DMNS=0.50996303*Q3
WRITE(3,141)
141 FORMAT( " ")
WRITE(3,142)
142 FORMAT( " ")
WRITE(3,143)
143 FORMAT( " ")
WRITE(3,145)
145 FORMAT( " ")
WRITE(3,150) Q1
150 FORMAT( " BEST LEAST SQUARES VALUE = ",F15.12)
WRITE(3,160) Q2
160 FORMAT( " THETA+ = ",F10.7)
WRITE(3,170) Q3
170 FORMAT( " THETA- = ",F10.7)
WRITE(3,180) Q4
180 FORMAT( " A'+ = ",F7.4)
WRITE(3,190) Q5
190 FORMAT( " A'- = ",F7.4)
WRITE(3,200) DPLS
200 FORMAT( " DELTA+ = ",F10.7)
WRITE(3,210) DMNS
210 FORMAT( " DELTA- = ",F10.7)
20 STOP
END

```

C SUBROUTINE FOR CALCULATING THE SUM OF SQUARES OF THE RESIDUALS FOR THE  
C CURRENT ESTIMATES OF THE ADJUSTABLE PARAMETERS

```

SUBROUTINE FUNCT1(N,XC,FC)
COMMON/PARAM/GAMMA(101),T(101),R(101)
EXTERNAL FUN
REAL Q,FC
INTEGER N
REAL XC(N)
REAL X1,X2,X3,X4
X1=XC(1)
X2=XC(2)
X3=XC(3)
X4=XC(4)
FC=0.0
DO75 I=1,101
    Q=(GAMMA(I)-(0.01*X3*EXP(-6.0E06*X1*T(I))+0.01*X4
+ *EXP(-6.0E06*X2*T(I))))**2.0
    FC=FC+Q
75 CONTINUE
RETURN
END

```

Program 6

C FOURIER TRANSFORM SOLUTION OF THE LAPLACE INTEGRAL EQUATION METHOD OF  
 C GARDNER, GARDNER, LAUSH AND MEINKE (1959)

C S = BIREFRINGENCE (RADS), GM = INTEGRAND OF EQUATION , G = G(EXP(-Y))  
 C T = TIME (SEC), R = TIME (NS), EC AND ES ARE THE ERROR ESTIMATES IN FC  
 C AND FS RESPECTIVELY DUE TO THE NUMERICAL INTEGRATION IN EQN. 125  
 C AND ER IS THE ERROR ESTIMATE DUE TO THE NUMERICAL INTEGRATION IN  
 C EQN. 128

C \*\*\*\*  
 C LOGARITHMIC TIME INCREASE, 140 DATA PTS.  
 C .001 DEGREES S.E.

C RANDOM NUMBER RUN 2

C \*\*\*\*  
 C PROTEIN 2

C \*\*\*\*  
 C PROGRAM MAIN(INPUT,OUTPUT,TAPE2=INPUT,TAPE3=OUTPUT)  
 C EXTERNAL FUNXN

C REAL MMU(66),KC(66),KS(66),FC(66),FS(66),GM(66),MU

C REAL YYY,G(690),Y(690),EC(66),ES(66)

C INTEGER N,I,IFAIL

C INTEGER L

C REAL X(141),S(141),R(141),T(141),YC(141),YS(141)

C COMPLEX Z,C,K,CGAMMA

C P=-7.1

C DO21 I=1,141

C P=P+.1

C WRITE(3,500)

500 FORMAT(" ")

C X(I)=P

C T(I)=(1.0E-09)\*EXP(X(I))

C R(I)=T(I)\*1.0E09

21 CONTINUE

C WRITE(3,32)

32 FORMAT(" TIME(NS) X S(T) = S(EXP(-X))")

501 FORMAT(" ")

C WRITE(3,502)

502 FORMAT("\*\*\*\*\*")

C WRITE(3,503)

503 FORMAT(" ")

C G05BBF REINITIALIZES THE STREAM OF THE RANDOM NUMBERS

C CALL G05BBF

C DO50 I=1,141

C CALCULATE THE UNPERTURBED DECAY CURVE

C S(I)=0.07\*EXP(-T(I)\*4.6596278E07)+

C +0.05\*EXP(-T(I)\*3.137407E07)

C NOW PERTURB EACH OF THE 140 DATA PTS USING A NORMAL PSEUDO-RANDOM  
 C NUMBER GENERATOR

C S(I)=S(I)+((0.1\*1.74555E-04)\*G05ADF(Y))

C WRITE(3,33)R(I),X(I),S(I)

33 FORMAT(F10.5,F6.2,F8.5)

50 CONTINUE

C DO47 L=1,20

C WRITE(3,504)

504 FORMAT(" ")

47 CONTINUE

C THE NEXT PART OF THE PROGRAM EVALUATES THE FOURIER TRANSFORM OF THE DATA

C MU=-.1

C WRITE(3,99)

99 FORMAT(" MU KC KS")

C WRITE(3,505)

C WRITE(3,506)

506 FORMAT("\*\*\*\*\*")

C WRITE(3,507)

507 FORMAT(" ")

C DO10 J=1,66

C MU=MU+.1

C MMU(J)=MU

C DO51 I=1,141

C YC(I)=(EXP(X(I)))\*S(I)\*COS(MU\*X(I))

C YS(I)=(EXP(X(I)))\*S(I)\*SIN(MU\*X(I))

C Y(I)=CMPLX(YC(I),YS(I))

51 CONTINUE

C N=141

C IFAIL=1

```

C CALL NUMERICAL INTEGRATION ROUTINE FROM THE UK NAG LIBRARY (MK 6)
CALL D01GAF(X,YC,N,ANS,ER,IFAIL)
FC(J)=((1.0/(2.0*3.141593))**0.5)*ANS
EC(J)=((1.0/(2.0*3.141593))**0.5)*ER
CALL D01GAF(X,YS,N,ANS,ER,IFAIL)
FS(J)=((1.0/(2.0*3.141593))**0.5)*ANS
ES(J)=((1.0/(2.0*3.141593))**0.5)*ER
C EVALUATE THE COMPLEX GAMMA FUNCTION FOR THE CURRENT VALUE OF MU USING
C THE SUBROUTINE BELOW
Z=CMPLX(1.0,MU)
C=CGAMMA(Z)
C DETERMINE THE EULER INTEGRAL OF THE COMPLEX GAMMA FUNCTION (EQN. 123 )
K=((1.0/(2.0*3.141593))**0.5)*C
KC(J)=REAL(K)
KS(J)=AIMAG(K)
C=CGAMMA(Z)
WRITE(3,101)MU,K
101 FORMAT( 7X,1F8.2,2E15.7)
10 CONTINUE
D049 L=1,20
WRITE(3,509)
509 FORMAT( "")
49 CONTINUE
WRITE(3,90)
90 FORMAT( "      MU      FC      (ERR)      FS
+      (ERR)" )
WRITE(3,510)
510 FORMAT( "")
WRITE(3,511)
511 FORMAT( *****
+*****")
WRITE(3,512)
512 FORMAT( "")
D038 J=1,66
WRITE(3,91)MMU(J),FC(J),EC(J),FS(J),ES(J)
91 FORMAT( 1X,1F8.2,4E14.7)
38 CONTINUE
D052 L=1,20
WRITE(3,513)
513 FORMAT( "")
52 CONTINUE
WRITE(3,93)
93 FORMAT( "      Y      G(EXP(-Y))      ERROR")
WRITE(3,514)
514 FORMAT( "")
WRITE(3,515)
515 FORMAT( "*****")
WRITE(3,516)
516 FORMAT( "")
YYY=-.01
D031 M=1,690
YYY=YYY+.01
Y(M)=YYY
D029 J=1,66
C DIVIDE THE FOURIER TRANSFORM OF THE DATA BY THE EULER INTEGRAL FOR THE
C COMPLEX GAMMA FUNCTION
GM(J)=(((FC(J)*KC(J))+(FS(J)*KS(J)))*COS(YYY*MMU(J)))/((KC(J)
+*KC(J))
++(KS(J)*KS(J)))+(((FS(J)*KC(J))-(FC(J)*KS(J)))*SIN(YYY*MMU(J))/(
+((KC(J)*KC(J))+(KS(J)*KS(J))))
29 CONTINUE
NN=66
C NOW G(EXP(-Y)) AS A FUNCTION OF Y IS FOUND FROM THE INVERSE FOURIER
C TRANSFORM USING THE SAME NUMERICAL INTEGRATION ROUTINE
CALL D01GAF(MMU,GM,NN,ANS,ER,IFAIL)
G(M)=(1.0/3.141593)*ANS
ER=(1.0/3.141593)*ER
WRITE(3,290)YYY,G(M),ER
IF(IFAIL)241,261,241
241 WRITE(3,289)
261 CONTINUE
290 FORMAT(/3X,F7.2,4X,1E15.7,4X,1E15.7)
289 FORMAT(/28H LESS THAN 4 POINTS SUPPLIED)
31 CONTINUE
C HENCE A PLOT OF G(EXP(-Y)) AGAINST Y IS OBTAINED
CALL PAPER(1)
CALL MAP(0.0,0.0,0.0,0.0)
CALL CURVE0(Y,G,1,690)
CALL SCALES
CALL BORDER
CALL GRAPHF(FUNXN)

```

```
CALL GREND
STOP
END
```

```
C
FUNCTION FUNXN(X)
FUNXN=0.0
RETURN
END
```

```
C SUBROUTINE FOR CALCULATING THE COMPLEX GAMMA FUNCTION C = CGAMMA(Z) FOR
C THE CURRENT VALUE OF MU. THIS SUBROUTINE IS THAT GIVEN BY LUCAS AND
C TERRILL (1970)
COMPLEX FUNCTION CGAMMA(Z)
COMPLEX Z,ZM,T,TT,SUM,TERM,DEN,PI,A
DIMENSION C(12)
LOGICAL REFLEX
C SET IOUT FOR PROPER OUTPUT CHANNEL OF COMPUTER SYSTEM FOR
C ERROR MESSAGES
IOUT=3
PI=(3.141593,0.0)
X=REAL(Z)
Y=AIMAG(Z)
C TOL = LIMIT OF PRECISION OF COMPUTER SYSTEM IN SINGLE PRECISION
TOL=1.0E-07
REFLEX=.TRUE.
C DETERMINE WHETHER Z IS TOO CLOSE TO A POLE
C CHECK WHETHER TOO CLOSE TO ORIGIN
IF(X.GE.TOL) GO TO 20
C FIND THE NEAREST POLE AND COMPUTE DISTANCE TO IT
XDIST=X-INT(X-.5)
ZM=CMPLX(XDIST,Y)
IF(CABS(ZM).GE.TOL)GOTO 10
C IF Z IS TOO CLOSE TO A POLE, PRINT ERROR MESSAGE AND RETURN
C WITH CGAMMA=(1.E7,0.F0)
WRITE (IOUT,900)Z
CGAMMA=(1.E7,0.E0)
RETURN
C FOR REAL(Z) NEGATIVE EMPLOY THE REFLECTION FORMULA
C GAMMA(Z)=PI(SINPI*Z)*GAMMA(1-Z)
C AND COMPUTE GAMMA(1-Z). NOTE REFLEX IS A TAG TO INDICATE THAT
C THIS RELATION MUST BE USED LATER.
10 IF(X.GE.0.0)GOTO 20
REFLEX=.FALSE.
Z=(1.0,0.0)-Z
X=1.0-X
Y=-Y
C IF Z IS NOT TOO CLOSE TO A POLE, MAKE REAL(Z)>10 AND ARG(Z)<PI/4
20 M=0
40 IF(X.GE.10.)GOTO 50
X=X+1.0
M=M+1
GOTO 40
50 IF(ABS(Y).LT.X)GOTO 60
X=X+1.0
M=M+1
GOTO 50
60 T=CMPLX(X,Y)
TT=T*T
DEN=T
```

```

C COEFFICIENTS IN STIRLING'S APPROXIMATION FOR LN(GAMMA(T))
C(1)=1./12.
C(2)=-1./360.
C(3)=1./1260.
C(4)=-1./1680.
C(5)=1./1188.
C(6)=-691./36060.
C(7)=1./156.
C(8)=-3617./122400.
C(9)=43867./244188.
C(10)=-174611./125400.
C(11)=77683./5796.
SUM=(T-(.5,0.0))*CLOG(T)-T*CMPLX(.5*ALOG(2.*3.14159),0.0)
J=1
70 TERM=C(J)/DEN
C TEST REAL AND IMAGINARY PARTS OF LN(GAMMA(Z)) SEPARATELY FOR
C CONVERGENCE. IF Z IS REAL SKIP IMAGINARY PART OF CHECK.
IF(ABS(REAL(TERM)/REAL(SUM)).GE.TOL)GOTO 80
IF(Y.EQ.0.0)GOTO 100
IF(ABS(AIMAG(TERM)/AIMAG(SUM)).LT.TOL)GOTO 100
80 SUM=SUM+TERM
J=J+1
DEN=DEN*TT
C TEST FOR CONVERGENCE
IF(J.EQ.12)GOTO 90
GOTO 70
C STIRLING'S SERIES DID NOT CONVERGE. PRINT ERROR MESSAGE AND
C PROCEDE
90 WRITE(IOUT,910)Z
C RECURSION RELATION USED TO OBTAIN LN(GAMMA(Z))
C     LN(GAMMA(Z))=LN(GAMMA(Z+M)/(Z*(Z+1)*...*(Z+M-1)))
C     =LN(GAMMA(Z+M)-LN(Z)-LN(Z+1)-...-LN(Z+M-1))
100 IF(M.EQ.0)GOTO 120
D0110 I=1,M
A=CMPLX(I*1.-1.,0.0)
110 SUM=SUM-CLOG(Z+A)
C CHECK TO SEE IF REFLECTION FORMULA SHOULD BE USED
120 IF(REFLEX)GOTO 130
SUM=CLOG(PI/CSIN(PI*Z))-SUM
Z=(1.0,0.0)-Z
130 CGAMMA=CEXP(SUM)
RETURN
900 FORMAT(1X,2F14.7,10X,49HARGUMENT OF GAMMA FUNCTION IS TOO CLOSE TO
+ A POLE)
910 FORMAT(44H ERROR - STIRLING'S SERIES HAS NOT CONVERGED/14X,4H7 ,
END

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Program 7

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C R-CONSTRAINED NON-LINEAR LEAST SQUARES METHOD (HARDING)
C
C GAMMA = BIREFRINGENCE (RAD/S), FC = SUM OF SQUARES OF THE RESIDUALS
C X(1) = CURRENT INITIAL GUESS FOR A/B
C X(2) = " " " " A+
C X(3) = " " " " A-
C ON EXIT, X(1), X(2), X(3) CONTAIN THE BEST ESTIMATES FOR THESE PARAMETERS
C XC(1) = A = CURRENT ESTIMATE FOR A/B
C D = 1/C = VALUE OF B/C CORRESPONDING TO THIS ESTIMATE
C S = " " VISCOSITY INCREMENT "
C V = " " DELTA+
C W = " " DELTA-
C THPLUS = " " THETA+
C THMNUS = " " THETA-
C XC(2) = CURRENT ESTIMATE FOR A+
C XC(3) = " " A-
C AA1,AA2,...,AA6 ARE THE A/B COORDINATES FOR 6 PTS ON THE R-CURVE
C AD1,AD2,...,AD6 B/C
C THE VALUE FOR B/C CORRESPONDING TO THE CURRENT ESTIMATE FOR A/B CAN THEN
C BE FOUND USING A CUBIC POLYNOMIAL INTERPOLATION PROCEDURE BETWEEN THE
C SIX GIVEN POINTS. THIS IS DONE USING A LIBRARY ROUTINE E01LF1
C ****
C PROTEIN 1
C *****
C LINEAR TIME INCREASE, 100PTS.
C CUT OFF TIME: 100NS
C STREAM OF RANDOM NUMBERS: 3
C 0.1 DEG STANDARD ERROR ON EACH DATA PT.

PROGRAM MAIN(INPUT,OUTPUT,TAPE2=INPUT,TAPE3=OUTPUT)
COMMON/PARAM/GAMMA(101),T(101),A,C,D,NN,AA(6),AD(6)
REAL R(101)
REAL AA1,AA2,AA3,AA4,AA5,AA6,AD1,AD2,AD3,AD4,AD5,AD6
REAL BL(3),BU(3),X(3),F,W(39)
INTEGER IBOUND,IFAIL,J,LIW,LW,N
INTEGER IW(5)
REAL Q1,Q2,Q3,Q4
WRITE(3,37)
37 FORMAT(" PROTEIN 1, 0.1 DEG. STANDARD ERROR")
WRITE(3,38)
38 FORMAT(
+ 100NS, 100PTS")
WRITE(3,39)
39 FORMAT(
+STREAM 3")
P=-1.1
D021 I=1,101
P=P+1.1
R(I)=P
T(I)=R(I)*1.0E-09
R(I)=T(I)*1.0E09
21 CONTINUE
C G05BAF(0,X) SPECIFIES THE XTH STREAM OF THE RANDOM NUMBERS
CALL G05BAF(0.3)
D050 I=1,101
C CALCULATE THE UNPERTURBED DECAY CURVE
GAMMA(I)=0.07*EXP(-T(I)*6.0*5.815383E06) +
+0.05*EXP(-T(I)*6.0*4.1564612E06)
C NOW PERTURB EACH OF THE 100 DATA POINTS USING A NORMAL PSEUDO RANDOM
C NUMBER GENERATOR G05ADF
GAMMA(I)=GAMMA(I)+((1.74555E-03)*G05ADF(Y))
50 CONTINUE
C READ IN THE VALUES FOR THE LOWER LIMITS FOR THE INITIAL GUESSES OF THE
C A/B, A+, A- (X100), THE LOWER AND UPPER LIMITS FOR THE COMPUTER ESTIMATES
C THE COORDINATES OF THE A/B VALUES AND THEN THE COORDINATES OF THE B/C
C FOR THE R-CURVE TO WHICH THESE ESTIMATES ARE CONSTRAINED
READ(2,*) XX1,XX2,XX3,BBL1,BBL2,BBL3,BBU1,BBU2,BBU3,
+AA1,AA2,AA3,AA4,AA5,AA6,AD1,AD2,AD3,AD4,AD5,AD6
AA(1)=AA1
AA(2)=AA2
AA(3)=AA3
AA(4)=AA4
AA(5)=AA5
AA(6)=AA6
AD(1)=AD1
AD(2)=AD2
AD(3)=AD3
AD(4)=AD4
AD(5)=AD5

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```

AD(6)=AD6
N=3
IBOUND=0
Q1=1.0
D010 I=1,3
Z=G05AAF(X)
X(1)=XX1+0.2*Z
X(2)=XX2+2.0*Z
X(3)=XX3+2.0*Z
BL(1)=BBL1
BL(2)=BBL2
BL(3)=BBL3
BU(1)=BBU1
BU(2)=BBU2
BU(3)=BBU3
LIW=5
LW=39
IFAIL=1
CALL E04JAF(N,IBOUND,BL,BU,X,F,IW,LIW,W,LW,IFAIL)
IF(IFAIL.NE.0)WRITE(3,100)IFAIL
IF(IFAIL.EQ.1)GOTO 20
100 FORMAT("ERROR EXIT TYPE",I3,"SEE ROUTINE MANUAL")
X(2)=X(2)*.01
X(3)=X(3)*.01
WRITE(3,110)F
WRITE(3,120)(X(1),X(2),X(3))
110 FORMAT(" FUNCTION VALUE ON EXIT IS",F15.12)
120 FORMAT(" A/B =",F8.5," A+=",F15.12,
+" A-=",F15.12)
IF(Q1.LE.F)GOTO 30
Q1=F
Q2=X(1)
Q3=X(2)
Q4=X(3)
30 CONTINUE
WRITE(3,130)
130 FORMAT(" ")
WRITE(3,140)
140 FORMAT(" ")
10 CONTINUE
WRITE(3,150)Q1
150 FORMAT(" BEST LEAST SQUARES VALUE = ",F15.12)
WRITE(3,160)Q2
160 FORMAT(" A / B = ",F8.5)
WRITE(3,170)Q3
170 FORMAT(" B / C = ",F8.5)
WRITE(3,180)Q3
180 FORMAT(" A+ = ",F7.4)
190 FORMAT(" A- = ",F7.4)
20 STOP
END

```

C  
C SUBROUTINE FOR CALCULATING THE SUM OF THE SQUARES OF THE RESIDUALS FOR  
C CURRENT ESTIMATES OF A/B, A+ AND A-  
C KB = BOLTZMANN'S CONSTANT, NA = AVOGADROS NUMBER

SUBROUTINE FUNCT1(N,XC,FC)  
COMMON/PARAM/GAMMA(101),T(101),A,C,D,NN,AA(6),AD(6)  
EXTERNAL FUN  
REAL Q,FC  
INTEGER N  
DIMENSION ALPHA(9)  
REAL XC(N)  
REAL X2,X3  
REAL THPLUS,THMNUS,TEMP,ETA,M,O,P,KB,NA,MW  
NN=0  
A=XC(1)  
NM=6  
IEXIT=0  
C CALL LIBRARY ROUTINE FOR THE CUBIC POLYNOMIAL FIT TO THE R-CURVE POINTS  
C A LISTING OF THIS IS GIVEN BELOW  
CALL E01LF1(NM,AA,AD,A,D,IEXIT)  
C=1.0/D  
B=1.0  
D045 K=1,9  
AZ=0.0  
BZ=1000000  
NN=NN+1  
MAXDIV=50  
EPS=1.0E-08  
ACC=0.0  
IFAIL=0  
CALL D01AGF(AZ,BZ,FUN,MAXDIV,EPS,ACC,ANS,ERROR,NOFUN,IFAIL)  
ALPHA(NN)=ANS  
45 CONTINUE  
S=(1.0/(A\*B\*C))\*((4.0/15.0)\*((ALPHA(7)+ALPHA(8)  
+ +ALPHA(9))/((ALPHA(8)\*ALPHA(9)+ALPHA(9)\*ALPHA  
+ (7)+ALPHA(7)\*ALPHA(8)))+(1.0/5.0)\*(((ALPHA(2)  
+ +ALPHA(3))/((ALPHA(4)\*(B\*B\*ALPHA(2)+C\*C\*ALPHA(3)  
+ ))+((ALPHA(3)+ALPHA(1))/((ALPHA(5)\*(C\*C\*ALPHA(3)  
+ +A\*A\*ALPHA(1))))+((ALPHA(1)+ALPHA(2))/(ALPHA(6)  
+ +(A\*A\*ALPHA(1)+B\*B\*ALPHA(2)))))))  
M=(B\*B+C\*C)/(B\*B\*ALPHA(2)+C\*C\*ALPHA(3))  
O=(C\*C+A\*A)/(C\*C\*ALPHA(3)+A\*A\*ALPHA(1))  
P=(A\*A+B\*B)/(A\*A\*ALPHA(1)+B\*B\*ALPHA(2))  
Z=((A\*B\*C)/(12.0))\*(((1.0/M)+(1.0/O)+(1.0/P  
+ ))-(((1.0/M\*\*2.0)+(1.0/O\*\*2.0)+(1.0/P\*\*2.0))-  
+ ((1.0/(M\*O))+(1.0/(O\*P))+(1.0/(P\*M  
+ )))\*\*0.5))  
U=((A\*B\*C)/(12.0))\*(((1.0/M)+(1.0/O)+(1.0/P  
+ ))+(((1.0/M\*\*2.0)+(1.0/O\*\*2.0)+(1.0/P\*\*2.0))-  
+ ((1.0/(M\*O))+(1.0/(O\*P))+(1.0/(P\*M  
+ )))\*\*0.5))  
V=6.0\*U\*S  
W=6.0\*Z\*S  
C ENTER INTRINSIC VISCOSITY  
ETA=2.746  
C ENTER TEMPERATURE  
TEMP=293.0  
C ENTER MOLECULAR WEIGHT  
MW=71744.0  
KB=1.38046E-16  
NA=6.0248E23  
THPLUS=(NA\*KB\*100.0/6.0)\*(TEMP/(ETA\*MW))\*V  
THMNUS=(NA\*KB\*100.0/6.0)\*(TEMP/(ETA\*MW))\*W  
X2=XC(2)  
X3=XC(3)  
FC=0.0  
D075 I=1,101  
Q=(GAMMA(I)-(0.01\*X2\*EXP(-6.0\*THPLUS\*T(I))+0.01\*X3\*EXP  
+ (-6.0\*THMNUS\*T(I))))\*\*2.0  
FC=FC+Q  
75 CONTINUE  
RETURN  
END

```

C LEICESTER UNIVERSITY COMPUTER LIBRARY SUBROUTINE FOR A CUBIC
C POLYNOMIAL FIT TO A SET OF POINTS (K. BROOLIE)
C
C      SUBROUTINE E01LF1(N,AX,AY,X,Y,IEXIT)
C      DIMENSION AX(N),AY(N)
C      CHECK DATA POINTS ARE MONOTONICALLY INCREASING
C          IEXIT=1
C          DO 5 I=2,N
C              IF (AX(I).LE.AX(I-1)) RETURN
C          5 CONTINUE
C      CHECK THAT X IS A VALID POINT
C          IEXIT=2
C          IF ((AX(1)-X)*(AX(N)-X).GT.0) RETURN
C      LOCATE INTERVAL IN WHICH X LIES -
C          AX(J-1).LT.X.LE.AX(J)
C          IEXIT=0
C          Y=AY(1)
C          IF (X.EQ.AX(1)) RETURN
C          DO 10 I=2,N
C              J=I
C              IF (X.LE.AX(I)) GOTO 20
C          10 CONTINUE
C          20 CONTINUE
C              Y=AY(J)
C              IF (X.EQ.AX(J)) RETURN
C      ESTIMATE SLOPE AT AX(J-1)
C          CALL E011A(N,AX,AY,J-1,G1)
C      ESTIMATE SLOPE AT AX(J)
C          CALL E011A(N,AX,AY,J,G2)
C      CONSTRUCT INTERPOLATING CUBIC POLYNOMIAL IN INTERVAL
C          D=AY(J-1)
C          C=G1
C          H=AX(J)-AX(J-1)
C          S=(AY(J)-AY(J-1))/H
C          B=(3.0*S-2.0*G1-G2)/H
C          A=(G1+G2-2.0*S)/H/H
C      EVALUATE POLYNOMIAL AT POINT
C          H=X-AX(J-1)
C          Y=((A*H+B)*H+C)*H+D
C          RETURN
C          END
C          SUBROUTINE E011A(N,AX,AY,J,G)
C          DIMENSION AX(N),AY(N)
C      CALCULATE SLOPES ON EITHER SIDE OF DATA POINT
C          JM1=J-1
C          JP1=J+1
C          IF (J.NE.1) GO TO 20
C      END-POINT IS DIFFERENT
C          H1=AX(2)-AX(1)
C          S1=2.0*(AY(2)-AY(1))/H1-(AY(3)-AY(2))/(AX(3)-AX(2))
C          GO TO 30
C          20 CONTINUE
C          H1=AX(J)-AX(J-1)
C          S1=(AY(J)-AY(JM1))/H1
C          30 CONTINUE
C          IF (J.NE.N) GO TO 40
C      END-POINT IS DIFFERENT
C          H2=AX(N)-AX(N-1)
C          S2=2.0*(AY(N)-AY(N-1))/H2-(AY(N-1)-AY(N-2))/(AX(N-1)-AX(N-2))
C          GO TO 50
C          40 CONTINUE
C          H2=AX(JP1)-AX(J)
C          S2=(AY(JP1)-AY(J))/H2
C          50 CONTINUE
C          S12=S1*S2
C      IF DATA IS NOT MONOTONIC SET SLOPE TO ZERO
C          IF (S12.GT.0.0) GO TO 10
C          G=0.0
C          RETURN
C          10 CONTINUE
C      WHEN DATA IS MONOTONIC USE WEIGHTED AVERAGE OF NORMAL SLOPES
C          T1=2.0*H1+H2
C          T2=H1+2.0*H2
C          T=(T1*S2+T2*S1)/(3.0*(H1+H2))
C          G=S12/T
C          RETURN
C          END

```

C  
C SUBROUTINE FOR CALCULATING THE ELLIPTIC INTEGRALS USED FOR DETERMINING  
C THE S VALUE FROM THE CURRENT GUESS FOR A/B

```

REAL FUNCTION FUN(Y)
COMMON/PARAM/GAMMA(101),T(101),A,C,D,NN,AA(6),AD(6)
B=1.0
GOTO(10,20,30,40,50,60,70,80,90),NN
10 FUN=1.0/((A*A+Y)**1.5*(B*B+Y)**0.5*(C*C+Y)**0.5)
RETURN
20 FUN=1.0/((A*A+Y)**0.5*(B*B+Y)**1.5*(C*C+Y)**0.5)
RETURN
30 FUN=1.0/((A*A+Y)**0.5*(B*B+Y)**0.5*(C*C+Y)**1.5)
RETURN
40 FUN=1.0/((A*A+Y)**0.5*(B*B+Y)**1.5*(C*C+Y)**1.5)
RETURN
50 FUN=1.0/((A*A+Y)**1.5*(B*B+Y)**0.5*(C*C+Y)**1.5)
RETURN
60 FUN=1.0/((A*A+Y)**1.5*(B*B+Y)**1.5*(C*C+Y)**0.5)
RETURN
70 FUN=Y/((A*A+Y)**0.5*(B*B+Y)**1.5*(C*C+Y)**1.5)
RETURN
80 FUN=Y/((A*A+Y)**1.5*(B*B+Y)**0.5*(C*C+Y)**1.5)
RETURN
90 FUN=Y/((A*A+Y)**1.5*(B*B+Y)**1.5*(C*C+Y)**0.5)
RETURN
END

```

Results:

PROTEIN 1, 0.1 DEG. ABSOLUTE ERROR

110NS, 100PTS  
STREAM3

FUNCTION VALUE ON EXIT IS .000399962998  
A/B= 1.48309 A+= .070458728408 A-= .048831535604

FUNCTION VALUE ON EXIT IS .000399962998  
A/B= 1.48309 A+= .070458845275 A-= .048831534073

FUNCTION VALUE ON EXIT IS .00399962998  
A/B= 1.48309 A+= .070458881237 A-= .048831534081

BEST LEAST SQUARES VALUE = .000399962998  
A / B = 1.48309  
A+ = .0707  
A- = .0488